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Technical Report

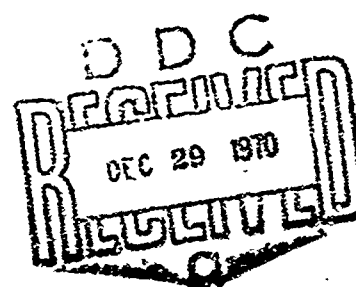
ANALYSIS OF DEEP WATER SINGLE POINT MOORINGS

by

John H. Nath
Associate Professor of Civil Engineering
Colorado State University

for

Office of Naval Research
Grant No. N00014-67-A-0229-0009



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Errata

The author has changed positions and is now:

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Page 19, Eq. (26), should read:

$$\zeta_{tt} = a^2 \zeta_{zz}$$

Page 20, the end of the second line below Eq. (30), should read:

$$B = Z_0 / \sin \frac{\omega L}{a}$$

Page 20, the third line from the bottom should read:

"is a surface following disc and the other is a non surface
following, or"

Page 33, the third word in the first line of the last paragraph should be:

"output"

Figure 42, in the caption the depth should be:

"Depth = 1000 FT. "

Technical Report

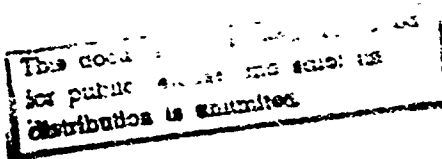
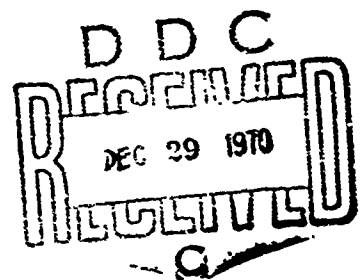
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ABSTRACT

Analytical and numerical studies were made of single point moorings of a large disc buoy in deep water. Waves of different frequencies and winds of different magnitudes were imposed on moorings of different scopes for nylon ropes. The numerical model results compared favorably with analytical solutions for a straight vibrating string and the buoy motion was validated with the results from a hydraulic model study. Approximate calculations, based on the straight vibrating string solution, were compared to the numerical results of curved mooring lines of various scopes. The analytical prediction of line tension was from fair to poor but the prediction of the position of the nodes of tension and the natural frequencies of the modes was good. A new method of presenting mooring line tension data in dimensionless form is presented that reduces moorings of different frequencies and line diameters to a common scale. The versatility of the numerical program was illustrated with two runs for moorings in shallow water with large waves in addition to a computation of line tension, position and velocity for the condition of a wind shift of 180 degrees on the buoy. The usefulness of the numerical program as a design tool was established.

ACKNOWLEDGMENTS

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The computer work was accomplished at the computer center at Colorado State University. Mr. W. W. Burt provided very able assistance on programming, particularly the plotting subroutines. Mr. Hin Fatt Cheong provided valuable assistance.

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INTRODUCTION

Background Information

This report will present the current status of research into the numerical analysis of the motion of the mooring line and buoy of a single point mooring in the deep ocean for an oceanographic buoy. The work originally started in the summer of 1967 for the Convair Division of General Dynamics and was continued in the summer of 1968. During the academic year 1968-1969 the work was continued by the author on a part time basis at Oregon State University under the auspices of the Office of Naval Research. Such a part time arrangement was continued during the past academic year, also for the Office of Naval Research. The objective of this study has been to develop a flexible numerical program that can be used for design work and for engineering research on the mooring of an oceanographic buoy in deep water with a single line. It was desired that the program be able to handle situations with relatively large slopes as well as taut moorings. The effects from waves, or problems on transients, such as the anchor last deployment procedure, can be studied. An alternative, or supplemental, approach would have been to consider a solution based on small perturbations about the equilibrium position of the line. However, such a procedure considers only sinusoidal input functions and the program that was developed was much more flexible in being able to compute results for a wide variety of problems which included certain non-linear effects. For design purposes it would be useful to have both types of solutions.

The numerical program can be considered to exist in two parts - one that determines the static or equilibrium position and tension in the line due to the action of wind, current and gravity and the second part that determines the dynamic tension and motion of the line due to waves or other forcing functions. The first part generates the initial conditions for the second part. All loads and system responses are considered to be acting in one plane.

The static part of the work has been described in Refs. 10 and 11 and the dynamic portion of the program has been described in Refs. 11 and 12.

The work has been successful to the point of developing and debugging a program which predicts the position, velocity and tension in all parts of the line and the buoy motion. The forcing function can be a wave of any form, providing the water particle velocities and accelerations are known as functions of water surface elevation. In addition, other transient problems can be studied, such as an anchor last deployment in still water, or a transient horizontal motion of the buoy due to a directional change in the wind. In many cases the internal or structural damping in the line has been considered as well as the hydrodynamic damping.

The differential equations of motion of the line have been derived in Ref. 12. The method of characteristics was used to set up the computational scheme for the numerical solution. Schram and Reyle (15) stated it well that the method of characteristics does not limit one to the consideration of small perturbations about the equilibrium. It was also shown in Ref. 12 how transfer functions can be developed and a general agreement was illustrated between a

computed transfer function and one developed from experimental work on a mooring in 13,000 feet of water near Bermuda.

Scope of This Study

This study continues to consider the co-planar or two-dimensional problem only. The buoy considered was the large discus buoy (forty feet in diameter) developed by General Dynamics for the Office of Naval Research. The mooring line characteristics are typical for man-made fibers, being non-linear in the stress-strain relationship. An approximation to line damping was included. Some time was required for additional debugging of the program from the 1969 results. It is felt that the program is highly developed now and can accomodate most, if not all, configurations of interest.

Favorable comparisons were made between the closed mathematical solutions for a relatively straight, vibrating string and the numerical model. Both longitudinal and transverse vibrations were considered.

Some recent laboratory experimentation with models by General Dynamics has resulted in data that enabled the author to validate the portion of the numerical model that predicts the prototype buoy motion due to different excitations. In addition, recent wind tunnel studies at Colorado State University have enabled a more accurate assessment of the wind drag forces on the buoy.

Of some interest of late has been the question of how the mooring line tension, and particularly that at the anchor, changes when a sudden 180 degree wind shift occurs at the buoy, holding all other variables constant. This problem was successfully studied and

it was determined that no unusual forces were exerted at the anchor that were not also distributed down the mooring line.

The primary interest in this research was to obtain some determination as to the influence on dynamic line tension due to line scope and the magnitude of the wind as well as the frequency of the waves. In addition, some minor runs were made at shallow depths to see how the mooring line behaved when a fairly large wave was subjected to the system.

It is felt that much more needs to be done in order to gain a complete view of the entire range of problems associated with the type of moorings that were studied. However, due to a real limitation in time and other resources it was necessary to leave the very interesting additional work to future studies.

Review of Recent Literature

Reference 12 presents a complete derivation of the equations of motion of the mooring line and buoy. The numerical solution of the equations indicated that the relationship between wave height and mooring line tension was somewhat linear for a wave period of 7.15 seconds. Hence, transfer functions, which relate the wave spectrum to the tension spectrum at a position on the line were developed for a simulated mooring representing real prototype conditions near Bermuda in 13,000 feet of water. General agreement was obtained between numerical predictions and field measured values of the transfer function. In addition, frequency response curves for the large disc buoy in the heave and pitch modes of motion were generated and it was estimated that the buoy was a nearly perfect surface follower for all wave frequencies up to 0.28 cps, where the response dropped

off sharply. Waves of higher frequencies provided very little stimulation to the buoy motion.

It is interesting to note that Devereux, et.al., (2) reported that line tension at the buoy was quite linearly related to wave height for waves of mixed frequencies for measurements taken at a prototype mooring in the Gulf Stream where the water depth was about 1040 feet and the length of nylon line plus chain was 1330 feet. The measurements were taken during Hurricane Betsy when the wave heights were as large as 30 to 50 feet and the predominant wave period was ten seconds.

The problem of predicting the static position of a buoy and mooring due to steady current has received considerable interest. Nath and Felix (10) presented basic equations and developed a numerical solution based on equal increments of tangency angle. Berteaux (1) also presents the basic equations and typical current profiles to be used off the East Coast of the United States and he presents some comparative results of calculations which study the influence of line diameter and scope on mooring design. Martin (7) describes a numerical program based on equal line segments and gives information on experimental drag forces on some buoy shapes. The report is mainly concerned with mooring lines that have steel rope for the upper portion to resist fish bite and nylon rope for the lower portion.

Treatments of the problem of solving for the dynamic tensions in different types of moorings have been developing in recent years. Nath (12) describes the foundations for the present study. Fofonoff and Garrett (4) developed approximate theoretical computations based on drag forces acting on the upper portion only of taut moorings. They were also concerned with the transient forces due to the anchor

last launching technique. Millard (9) presents static tension variations and particularly dynamic tension variations wherein the dynamic tension variations were very roughly proportional to the wind speed. He attributed that behavior to the increased sea state for higher winds but this report will show that it is also reasonable to attribute at least a large portion of the increased dynamic tension to the increased mean line tension.

Goeller and Laura (6) present equations of motion for closed solutions in complex form for straight compound lines where the central interest is in salvage, or raising loads from the ocean floor. They included concepts of internal damping in the line, comparing the results of a simple distributed mass having the usual two parameter model of damping with a lumped mass three parameter model. Experiment and theory showed that the simple treatment yielded good results in the region of resonance; where the effects of damping are most important.

Schram and Reyle (15) used the method of characteristics transformation to the partial differential equations for a flexible line to develop a three-dimensional numerical solution for the dynamic response of cable towed systems at sea. They considered the cable to be inextensible and they did not consider hydrodynamic added mass. Since the modulus of elasticity of the material was not considered, the slope of all characteristic curves were equal to the velocity of a displacement wave on the line. Nath (12) showed that the slope of two of the four characteristic curves were equal to the celerity of a longitudinal elastic wave in the line. The cable

towed systems illustrated that the transverse motion was damped to a much greater degree than the longitudinal motion.

The anchor last deployment procedure for buoy moorings was investigated by Froidevaux and Scholten (5). The analysis for numerical solution utilized a lumped mass representation of the line. The analysis was done for a short system and the results were extrapolated for a larger one. When the elasticity of the line was introduced into the solution a prohibitive amount of computer time was encountered.

A major unknown in the analysis of buoy mooring systems has been the hydrodynamic drag and added mass characteristics of the buoys. Mercier (8) describes an experimental model study on various buoy shapes in a wave basin and Felix (3) describes a model study for the large disc buoy.

THEORETICAL CONSIDERATIONS

This section will present a summary of the final developments of the scheme for the numerical modeling for a single point mooring of the large ONR disc buoy. The assumed line is a typical nylon plaited rope with a non-linear stress-strain diagram and simple two parameter damping, which is inversely proportional to the frequency, will be used.

Governing Equations for Line Motion

The derivations for the governing equations for the line motion are given in Ref. (12). The method of characteristics was utilized to transform the partial differential equations to total differential equations. The four dependent variables involved are the velocity of the line taken in the axial direction, which is tangent to the curvature of the line, v_a , the velocity of the line taken in the radial direction, which is perpendicular to the line tangent, v_r , the angle the line tangent makes with the horizontal, θ , and the line tension, T . The two independent variables are the distance, s , measured along the line from the coordinate axes as shown in Fig. 1, and the time, t . The solution proceeds numerically on an imaginary s - t grid composed of equal time increments, Δt , and distance increments, Δs , (except at the upper boundary condition, which is described later). Illustrations and a description of the procedures are given in Ref. 12.

The finite difference form of the total differential equations can be expressed with the following matrix equation.

On the
characteristic
curve

$$\begin{bmatrix} 1 & 0 & -v_r^{(1)} & -\frac{1}{C_a^{(1)}\nu} \\ 1 & 0 & -v_r^{(1)} & +\frac{1}{C_a^{(1)}\nu} \\ 0 & 1 & (v_a^{(1)} - C_r^{(1)}) & 0 \\ 0 & 1 & (v_a^{(1)} + C_r^{(1)}) & 0 \end{bmatrix} \begin{bmatrix} v_a^{(2)} \\ v_r^{(2)} \\ \theta^{(2)} \\ T^{(2)} \end{bmatrix} = \begin{bmatrix} f_1 \\ f_2 \\ f_3 \\ f_4 \end{bmatrix} \quad \left\{ \begin{array}{l} \frac{ds}{dt} = \left(\frac{AE}{\nu}\right)^{1/2} \\ -\left(\frac{AE}{\nu}\right)^{1/2} \\ \left(\frac{T}{M}\right)^{1/2} \\ -\left(\frac{T}{M}\right)^{1/2} \end{array} \right. \quad (1)$$

Wherein the f terms represent the forcing functions on the line. The superscript 2 stands for the values at $t+\Delta t$ and the superscript 1 stands for the values at time t . That is, the coefficient matrix contains the values of v , etc., at time t .

In Eq. 1,

$$C_a = \left(\frac{AE}{\nu}\right)^{1/2} \quad (2)$$

and

$$C_r = \left(\frac{T}{M}\right)^{1/2} \quad (3)$$

where A is the cross-sectional area of the line, E is the modulus of elasticity, or the slope of the tangent to the stress-strain diagram of the line, ν is the saturated mass density of the line in slugs per foot and M is the virtual mass of the line per foot (the

actual mass plus the hydrodynamic added mass). For completeness, the forcing functions will be listed below.

$$f_1 = - \Delta t g \left(1 - \frac{1}{G}\right) \sin\theta + v_a - v_r \theta - \frac{\tau}{C_a \mu} - \frac{C_a Q}{E} \Delta t \frac{\partial^2 \epsilon}{\partial t^2} \quad (4)$$

$$f_2 = - \Delta t g \left(1 - \frac{1}{G}\right) \sin\theta + v_a - v_r \theta + \frac{\tau}{C_a \mu} + \frac{C_a Q}{E} \Delta t \frac{\partial^2 \epsilon}{\partial t^2} \quad (5)$$

$$f_3 = \Delta t \left[\frac{C_D}{\pi D} \left(\frac{2}{C_I + G} \right) V |V| + \left(\frac{1 + C_I}{G + C_I} \right) \left(A_z \cos\theta - A_x \sin\theta \right) - \left(\frac{G - 1}{G + C_I} \right) g \cos\theta \right] + v_r + (v_a - C_r) \theta \quad (6)$$

$$f_4 = \Delta t \left[\frac{C_D}{\pi D} \left(\frac{2}{C_I + G} \right) V |V| + \left(\frac{1 + C_I}{G + C_I} \right) \left(A_z \cos\theta - A_x \sin\theta \right) - \left(\frac{G - 1}{G + C_I} \right) g \cos\theta \right] + v_r + (v_a + C_r) \theta \quad (7)$$

In the above equations, g is the acceleration of gravity, G is the specific gravity of the saturated line, Q is the damping coefficient which will be described later, ϵ is the strain in the line, C_D is the drag coefficient perpendicular to the line, D is the line diameter, C_I is the added mass coefficient (which is equal to 1.0 for a smooth circular cylinder), V is the relative velocity between the line and the water in the radial direction and A_z and A_x are the accelerations of the water particles in the z and x directions. The values of the variables in Eqs. 4 through 7 are determined at time t by an interpolation procedure from the s - t grid intersection points as described in Ref. 12. The second derivative of the line strain was determined simply with the finite

difference approximation,

$$\frac{\partial^2 \epsilon}{\partial t^2} \approx \frac{\epsilon_3 - 2\epsilon_2 + \epsilon_1}{(\Delta t)^2} \quad (8)$$

where the subscripts represent the preceding values of strain.

Governing Equations for Buoy Motion

The motion of the buoy was simply treated in terms of rigid body motion. All the forces acting on the buoy were considered in the x_2 and z_2 directions which are shown in Fig. 1. The acceleration of the buoy was determined at each time station with Newton's second law of motion and the displacement and velocity for the next time station was determined by means of recurrence formulae. The forces on the buoy were those due to pressure, or buoyancy, wind and current drag, added mass, line tension and gravity. The forces were summed in the x_2 and z_2 directions and moments were summed about the center of gravity. To approximate the true distribution of forces on the buoy the buoy was divided into a number of pie-shaped pieces. It was assumed that drag and added mass forces were concentrated near the lower chine of the buoy. By taking summation of forces in the x_2 direction equal to the mass of the buoy times the acceleration of the center of gravity in the x_2 direction and by subsequent re-arrangement the following equation can be derived.

$$K_1 \ddot{x}_2 + K_2 \dot{x}_2 = W_t \sin \phi + W_{x_2} - T_{x_2} + \Sigma p_{x_2} + F_{x_2} + C_{IR} \rho A_{x_2} \dot{x}_2 \quad (9)$$

And in the z_2 direction,

$$K_3 \ddot{z}_2 - K_4 \dot{\phi} = - Wt \cos \phi + W_{z2} - T_{z2} + Ep_{z2} + \sum F_{z2} + C_{IA} \rho \Sigma \gamma A_{z2} \quad (10)$$

Likewise, by taking summation of moments about the center of gravity equal to the moment of inertia about the center of gravity times the angular acceleration,

$$K_5 \ddot{x}_2 - K_4 \ddot{z}_2 + K_6 \ddot{\phi} = W_{x2} Z_2 + F_{x2} Z_1 + T_{x2} Z_3 + Ep(\text{mom. arms}) - \sum F_{z2} X_1 + C_{IR} \rho Z_1 A_{x2} \Sigma \gamma - C_{IA} \rho \Sigma \gamma A_{z2} X_1 + q \dot{\phi} \quad (11)$$

In the above equations $\dot{\phi}$ represents the derivative of ϕ with respect to time and $\ddot{\phi}$ is the second derivative. The coefficients on the left of the equations are,

$$K_1 = \frac{Wt}{g} + C_{IR} \rho \Sigma \gamma \quad (12)$$

$$K_2 = C_{IR} \rho Z_1 \Sigma \gamma \quad (13)$$

$$K_3 = \frac{Wt}{g} + C_{IA} \rho \Sigma \gamma \quad (14)$$

$$K_4 = C_{IA} \rho \Sigma \gamma X_1 \quad (15)$$

$$K_5 = C_{IR} \rho Z_1 \Sigma \gamma \quad (16)$$

$$K_6 = \bar{I} + C_{IR} \rho Z_1^2 \Sigma \gamma + C_{IA} \rho \Sigma \gamma X_1^2 \quad (17)$$

The definitions of the various terms in Eqs. 9 through 17 are:

Wt is the total buoy weight, W_{x2} is the wind force component in the x_2 direction, likewise for W_{z2} , T_{x2} and T_{z2} are the line force components, p is a pressure force on a pie-shaped piece of the buoy, the details of which will not be presented here, F_{x2} is the total wave and current drag force acting on the buoy in the x_2 direction

and it was assumed that it acted at a point mid-way between the attachment point and where the water surface profile intersects the z_2 axis, which was designated the distance Z_1 from the center of gravity, F_{z2} is the wave and current drag force acting on a pie-piece in the z_2 direction based on the relative velocity at the lower chine and acting at a distance X_1 from the center of gravity, parallel to the x_2 axis, C_{IR} is the inertia or added mass coefficient for the buoy in the radial, or x_2 direction, C_{IA} is the inertia coefficient in the axial or z_2 direction, ρ is the mass density of sea water, A_{x2} is the component of the acceleration of the water particles at Z_1 in the x_2 direction, A_{z2} is the acceleration of the water particles at the chine of a pie-piece, γ is the displacement volume of a pie-piece, Z_2 is the distance from the center of gravity to where the wind force is assumed to be concentrated, Z_3 is the distance from the center of gravity to the attachment point, (mom.arms) refers to the various moment arms from the center of gravity to the pressure forces on the pie-piece and q is a damping coefficient that was used in conjunction with $\dot{\phi}$ to provide the proper damping and period of the buoy as predicted by the numerical model in order that the pitch mode match the results of a hydraulic model study.

Boundary Conditions

At the anchor end of the line the velocities and displacements are set equal to zero for all time. Then the set of four equations and four unknowns as expressed in Eq. 19 reduce to two equations and two unknowns for determining the values of θ and T at the anchor.

The line is divided into a number of equal segments, Δs long, at time = 0. The segment lengths remain fixed in time except for the end segment which attaches to the buoy, the length of which is determined at each time increment. The number of segments can be increased or decreased according to whether the line is lengthening or shortening. The procedure is to use the method of characteristics to determine v_a , v_r , θ and T for all segments except the one next to the buoy. Knowing Δs and δ for each segment, the coordinates at the ends of each segment are determined. Since the coordinates of the attachment point at the buoy are known from the buoy motion subroutine, the length of the last segment can be determined, which also determines θ for the last segment. Knowing the distribution of tension in the line, the strain in each equal segment can be determined and since the total length of the line is known the strain in the end segment can be calculated, thence the end tension from the stress-strain diagram. The velocities of the end segment are determined from the buoy subroutine. More details on the above procedures are presented in Ref. 12.

PHYSICAL CHARACTERISTICS OF THE SYSTEM

This study considered mooring lines which are characterized by plaited nylon. Deep water depths were mostly considered because several harmonics of the resonant frequencies for such mooring conditions can exist. Line diameters of 2.0, 2.5 and 3.5 inches were used with scopes of 0.86, 0.87 and 1.18, where scope is the original unstretched length of the line divided by the water depth. Two conditions of wind and current were investigated. The winds were 50 knots and 150 knots and the corresponding current profiles that were assumed are shown in Fig. 2.

It is very difficult to determine the elongation characteristics for ropes made of synthetic fibers for a general study. Generally, polyester materials have less elongation than nylon for the same stress condition. However, the type of rope, twist-lay, plaited, etc., and the tightness of the strand will influence the load-elongation curves to a great degree, so that it is possible and it has occurred that certain types of nylon ropes will display less elongation than certain types of polyester ropes. Generally, of course, the reverse is true. In addition, the stress-strain characteristics are considerably influenced by submersion of the rope, yet practically no information exists on this topic. Thus, a designer has little information to work with unless tests can be performed, under water, on the very rope he plans to use. For this study it was assumed that the mooring rope was subject to an initial and permanent strain of 0.1 from the initial, or some subsequent, loading. The stress-strain diagram is presented in Fig. 3. Also on Fig. 3 are the results of some testing that are reported on in Martin (7) and Wilson

(15) and the stress-strain diagram used in Ref. 12. The final selection of the stress-strain diagram was somewhat influenced by test information provided by the Columbian Rope Company.

The internal hysteretic damping characteristics for the line were estimated from information given in Refs. 15 and 16. The procedure was to measure the area (thus the energy dissipated) of several hysteresis loops, approximate them as ellipses and utilize the following equations. For an elliptical hysteresis loop, the amplitude of the loading function P_0 , is related to the amplitude of the displacement, x_0 , and the phase shift, β , with:

$$\sin \beta = \frac{\text{Area within the ellipse}}{\pi P_0 x_0} \quad (18)$$

Thus, β can be determined. Simple linear damping in a continuous system is characterized by

$$\sigma(s,t) = E \epsilon(s,t) + Q \frac{\partial \epsilon}{\partial t} \quad (19)$$

or in a non-linear system (as considered in this report) by

$$\sigma(s,t) = \sigma(\epsilon) + Q \frac{\partial \epsilon}{\partial t} \quad (20)$$

where σ is the stress (calculated as the line tension divided by the original cross-sectional area of the line). E is the modulus of elasticity of the material, ϵ is the strain and Q is the damping coefficient. The damping coefficient, Q , can be estimated by considering the linear system, wherein

$$\tan \beta = \frac{Q\omega}{E_d} \quad (21)$$

where ω is the frequency of the forcing function and E_d is the

mean, or dynamic modulus of elasticity. Thus

$$Q = \frac{1}{\omega} E_d \tan \sin^{-1} \left(\frac{\text{Ellipse area}}{\pi P_o x_c} \right) \quad (22)$$

Thus from Refs. 15 and 16, Q was estimated to be

$$Q = \frac{4 \cdot 10^6}{\omega} \frac{\text{lb} \cdot \text{sec}}{\text{ft}^2} \quad (23)$$

For the solution of the numerical program the drag forces in the longitudinal direction on the line were ignored. It has been shown in several studies that they have negligible influence when scope is less than 2. The drag coefficient in the radial direction was taken equal to 1.4 and the added mass coefficient was given the theoretical value of 1.0 for a smooth circular cylinder. The saturated mass density of the line was developed as

$$\mu = 1.71 D^2 \quad (24)$$

where μ is the mass per foot and D is the line diameter in feet. Equation 24 was based on a saturated mass density of the line of 2.17 slugs per cubic foot.

A physical description of the buoy is presented in Ref. 12. Several coefficients were derived for the buoy from experimental information. The drag coefficient in the x_2 direction is a function of Froude number, but for the relative velocities considered here it was felt it could be assumed to be constant at 0.035. The added mass coefficient, C_{IR} , was 0.4.

In order to obtain similarity between the numerical model and the results of the hydraulic model study reported in Ref. 3 with respect to response decay curves, it was necessary to arbitrarily modify the

usual expression for drag force in the z_2 direction of the buoy by making the force proportional to the velocity instead of the velocity squared. In Eq. 10, F_{z_2} was established for one pie-piece as

$$F_{z_2} = C_{DA} \frac{\pi (40)^2}{4} \frac{1}{12} \frac{\rho}{2} V_{z_2} \quad (25)$$

Thus the drag coefficient is no longer dimensionless. For this work the value of C_{DA} was 12.0. The value when the relative acceleration in the z_2 direction at the chine was positive of C_{IA} was taken as 3.0, and 0.8 when that relative acceleration was negative. The auxiliary damping coefficient, q , in Eq. 11 was given the value 200,000 ft-lb-sec. The distance X , was determined to be 9.0. The dimensional wind drag coefficient, C_{Dw} , where $W = C_{Dw} \rho_{air} V_w^2 / 2$, was determined experimentally in Nath (13) to be 140. The resulting buoy motion due to the above selection of coefficients is given in the next section.

NUMERICAL RESULTS

Longitudinal and Transverse Motion of the Line

One way to check a numerical model such as the one presented here is to compare the results from it to those from a closed solution of a simplified problem. This was done for the case of a taut vibrating string, the solutions of which are well known. The development of the analytical solution will be presented first, followed by comparisons of analytical results with those from the numerical model.

Consider a straight, weightless line held vertically as shown in Fig. 4. The line has a cross-sectional area of A and a modulus of elasticity of E . The initial tension in the line is T_0 . At $z = L$ the line is forced with a longitudinal excitation, $Z_0 \sin \omega t$, where ω is the radian frequency of the excitation, and it is assumed that the initial tension is adequate to preserve the condition of positive tension in the line at all locations and times. It is assumed that the effects of damping are negligible. The vertical displacement of a particle of the line will be designated as ζ and the strain in the line is then ζ_z , where the subscript indicates the partial derivative with respect to z . Only the steady state vibration solution to the problem is desired. It is well known that the governing equation is the wave equation, which is:

$$\zeta_{tt} = a^2 \zeta_{zz} \quad (26)$$

where ζ_{tt} is the second derivative of the displacement with respect to time and a turns out to be the celerity of an elastic wave along the line also given by Eq. 2.

The displacement is then a function of the coordinate, z , and the time, t , and the boundary conditions are:

$$\zeta(0,t) = 0 \quad (27)$$

$$\zeta(L,t) = Z_0 \sin \omega t \quad (28)$$

It should be noted that $L \gg Z_0$ and that the problem has been linearized by imposing the boundary condition at $z = L$ instead of the true condition, $z = L + Z_0 \sin \omega t$. The solution is obtained by assuming that it is a product in the form:

$$\zeta(z,t) = (A \cos \frac{\omega}{a} z + B \sin \frac{\omega}{a} z) \sin \omega t \quad (30)$$

By imposing the first boundary condition it is seen that $A = 0$.

By imposing the second boundary condition it is seen that $B = Z_0 / \frac{\omega L}{a}$.

The solution for the displacement due to dynamic motion is then

$$\zeta(z,t) = Z_0 \frac{1}{\sin \frac{\omega L}{a}} \sin \frac{\omega z}{a} \sin \omega t \quad (31)$$

and for the strain:

$$\zeta_z(z,t) = Z_0 \frac{\omega}{a} \frac{1}{\sin \frac{\omega L}{a}} \cos \frac{\omega z}{a} \sin \omega t \quad (32)$$

Most ropes do not have linear elastic characteristics, but if they are stressed to at least 20% of their ultimate strength the stress strain diagram becomes approximately linear. The linear condition was assumed for this section of the work.

For a linear elastic material the strain is directly proportional to the stress through the modulus of elasticity, so that the solution for the dynamic line tension, T , is

$$T(z,t) = AE \sum_0 \frac{\omega}{a} \frac{1}{\sin \frac{\omega L}{a}} \cos \frac{\omega z}{a} \sin \omega t . \quad (33)$$

For the total tension the steady tension, T_0 , must be added to Eq. (33). By substituting Eq. 33 into Eqs. 26 through 28 it is seen that it is the solution desired for the steady state vibration condition.

Equation 33 shows that the line tension has infinite values where $\sin \frac{\omega L}{a} = 0$. This will occur when

$$\frac{\omega L}{a} = n \pi , \quad n = 1, 2, 3, \dots \quad (34)$$

(The case for $n = 0$ is a trivial case where either $L = 0$ or $\omega = 0$).

The numerical model was tested by modifying it to consider a linear elastic material with no damping and with longitudinal motion only. A frequency of 0.7 radians per second was used to represent ocean wave frequencies that can occur as strong swell. Several water depths, or lengths of line, were checked and Table 1 shows the results.

The line tensions were plotted by the computer for the anchor and the buoy end as functions of time. Examples of such plots are shown as Figs. 5 and 6. It was also seen by inspection of the printed output that nodes of zero tension fluctuation occurred at the positions on the line which are predicted by Eq. 33.

It was attempted to create a resonant condition by selecting a frequency such that $\omega L/a = 2\pi$. The purpose was to investigate the effects of internal damping on preventing infinite response as predicted by Eq. 33. However, even by setting the damping coefficient, Q , equal to zero, infinite response was not obtained, which

indicated that the numerical solution as presented was naturally damped. At this writing it has not been determined why the numerical solution as presented here is naturally damped.

It was also discovered that the full amount of damping, as predicted by Eq. 23, produced a numerical instability in the program. However, when one-tenth of the theoretical value of damping was used, the solution was stable for most conditions and it is felt that this degree of damping in conjunction with the natural damping will produce results that will approximate the action of a real nylon line. The results of testing the solution for a 20,000 feet long line are given in Table 2.

The results show that for the conditions assumed the oscillations in tension were reduced by one-third. For frequencies that were not near the resonant frequencies the damping had little influence on the oscillations, as expected.

The numerical model was also checked in the transverse, or x direction. In this case the steady state transverse vibration was determined for all positions, z , and time, t . The analysis assumed that displacements were very small and that the tension in the line was constant in time and position.

The assumed conditions were that both ends of the line remain fixed and at time equal to zero the transverse velocity of the line was sinusoidally distributed along the line. As time progressed the horizontal displacement of the line was also longitudinally distributed and the following development will show the closed solution for the horizontal displacement, $n(z,t)$. The boundary conditions for this problem are,

$$\eta(0,t) = \eta(L,t) = 0 \quad (35)$$

The initial condition is

$$\eta_t(z,0) = V_0 \sin \frac{\omega z}{b} \quad (36)$$

where V_0 is any convenient velocity amplitude and b is the longitudinal celerity of a displacement wave along the line given also by Eq. 3.

The governing equation is again the wave equation,

$$\eta_{tt} = b^2 \eta_{zz} \quad (37)$$

A product solution is assumed and the general form is

$$\eta(z,t) = (C \cos \frac{\omega}{b} z + D \sin \frac{\omega}{b} z) \sin \omega t \quad (38)$$

After applying the boundary conditions and the initial condition, the solution is found to be,

$$\eta(z,t) = \frac{V_0}{\omega} \sin \frac{\omega z}{b} \sin \omega t \quad (39)$$

Equation 39 shows that there are nodes on the line of zero displacement for all time. In the numerical program the tensions were set to be constant with time and position and all drag and added mass coefficients were set equal to zero.

For the numerical work, an initial tension of 3905.2 pounds was assumed in addition to a frequency, ω , of 0.251 rad/sec and a line length of 20,000 feet. It is seen, then, from Eq. 39 that nodes should occur in the line at $z = 5,000, 10,000, 15,000,$ and $20,000$ feet. The results of the numerical work showed that the nodes

occurred at about ω equal to 5400, 10,000, 15,400 and, of course, 20,000 feet.

The maximum magnitudes of the displacements should be 18.3 feet, as predicted by Eq. 39. Figure 7 shows that the displacements were not perfectly symmetrical, mostly due to the fact that the nodes did not occur exactly where they were supposed to occur. However, the average maximum displacement as determined from Fig. 7 is 18.3 feet.

The conclusion from the above tests was that the rating of the numerical model can be described as from good to excellent, the first rating applied to the transverse motion and the second referring to the longitudinal motion.

Many buoy moorings are established with a very taut line running almost vertically from the anchor to the buoy. It will be shown below that the resonant length or frequency of the mooring line will depend a great deal on the type of buoy that is used at the water surface.

One condition for consideration is that shown by Fig. 4 where the longitudinal displacement at the top of the line is imposed as the boundary condition. The equation of motion in terms of displacement is given by Eq. 31 and the line tension is given by Eq. 33. These equations show that resonant conditions exist when $\omega L/a = n\pi$.

Consider next equal conditions except that the boundary condition at the top of the line is a force given by

$$f_{z=L} = F_0 \sin \omega t \quad (40)$$

The new boundary conditions, for a material with a linear stress-strain relationship, are given by Eq. 40 and

$$\zeta_z(L, t) = \frac{1}{AE} F_0 \sin \omega t \quad (41)$$

On substitution of the boundary conditions into Eq. 30, one again finds that $A = 0$ and that

$$B \frac{\omega}{a} \cos \frac{\omega L}{a} \sin \omega t = \frac{1}{AE} F_0 \sin \omega t \quad (42)$$

thus,

$$B = \frac{F_0}{AE} \frac{a}{\omega} \frac{1}{\cos \frac{\omega L}{a}} \quad (43)$$

and the solution for displacements is,

$$\zeta(z, t) = \frac{F_0}{AE} \frac{a}{\omega} \frac{1}{\cos \frac{\omega L}{a}} \sin \frac{\omega z}{a} \sin \omega t \quad (44)$$

The curious difference between Eqs. 44 and 32, is that infinite responses occur for Eq. 32 at $\omega L/a = n\pi$ but for Eq. 44 they occur at $\omega L/a = n \frac{\pi}{2}$.

For design purposes the resonant conditions should be avoided. For very taut moorings that approximate the configuration shown in Fig. 4 the most serious mode of motion will probably be the longitudinal one. Damping may be relatively low. The resonant length of line, given a particular wave frequency, will then depend on the boundary condition at the top of the line.

Consider two types of buoys that may conceivably be moored to nearly vertical mooring lines at the air-water interface. One buoy is a surface following large disc and the other is a non surface, or relatively stable, spar. For a flexible mooring line the large disc will impose a displacement at the upper end of the line as it closely

follows the undulations of the water surface whereas the spar buoy will impose a time varying force on the line as the waves pass the spar. For a particular wave frequency the resonant length of line for the disc mooring will be

$$L = n \frac{\pi a}{\omega} \quad n = 1, 2, 2, \dots \quad (45)$$

For the spar buoy, the resonant length of mooring line will be

$$L = n \frac{\pi a}{2\omega} \quad n = 1, 3, 5, \dots \quad (46)$$

For other buoy types, such as the aid to navigation buoys used by the U. S. Coast Guard, some condition between Eqs. 45 and 46 will exist. In addition, several wave frequencies exist at sea and all resonant conditions with respect to the entire wave frequency spectrum should be investigated.

To illustrate with numbers the foregoing concepts, consider a common ocean wave period of seven seconds. The frequency will be 0.90 radians per second. Assume that a one-inch diameter nylon line (that is nearly neutrally buoyant) is used and that it is pre-stressed to 2200 pounds. The modulus of elasticity will be about 7.5×10^6 psf according to Fig. 3. The saturated density of the line will be about 0.0118 slugs per foot. Thus the celerity of a longitudinal elastic wave in the line will be about,

$$a = \sqrt{\frac{.00547 \times 7.5 \times 10^6}{0.0118}} \quad (47)$$

or,

$$a \approx 1860 \text{ fps} \quad (48)$$

For the disc buoy, the resonant lengths of mooring line will be 6,500 feet, 13,000 feet, etc. For the spar buoy, the resonant lengths of line will be 3,250 feet, 9,750 feet, etc. It should be stated again for emphasis that all wave frequencies should be examined for the resonant lengths of the line and the type of buoy must be given careful consideration.

Now consider the equations for line tension for both the above conditions. For the disc buoy the tension is given by Eq. 33. For the spar buoy the tension will be,

$$T(z,t) = F_0 \frac{1}{\cos \frac{\omega L}{a}} \cos \frac{\omega z}{a} \sin \omega t \quad (49)$$

For both conditions the dynamic line tension is a maximum at the anchor! For the disc buoy the dynamic tension at the buoy may be zero if $\omega L/a = n\pi/2$ with $n = 1, 3, 5, \dots$. For the spar buoy the dynamic line tension at the buoy will be $F_0 \sin \omega t$ and the displacement will be zero if $\omega L/a = n\pi$, $n = 1, 2, \dots$.

Buoy Motion

A necessary part of this study was to select the proper values of the coefficients in Eqs. 9 through 17. The procedure was to rely heavily on the 1:10 scale model study in Ref. 3. In particular some response decay curves for the pitch and heave motions were generated that implicitly display the effects of all the coefficients. By trial and error the coefficients were evaluated for the numerical model until the predicted response curves nearly matched the best estimate for the response curves of the prototype. The response curves for the prototype were estimated from the response curves from the scale

model study by considering the Froude modeling relationships and the shift in natural periods due to different degrees of damping. Hydrodynamic damping in the model studies should be greater than in the prototype because of the Reynolds number scale effect. The natural period in heave for the prototype predicted by the model study was about 3.6 seconds. After accounting for the Reynolds number effect, the period was reduced to 3.2 seconds. The period in heave from the numerical model was 3.1 seconds, which was considered to be close enough. Peaks in tension spectra from prototype measurements occur at periods of from 3.1 to 3.4 seconds and it is predicted here that they were due to the heaving motion of the buoy. The model study also showed a ratio of 1.128 between the heave period and the pitch period. The ratio for the numerical work is 1.148.

Figure 8 presents the normalized pitch response decay curve for the numerical work and the results from the hydraulic model study where the normalizing pitch is the pitch at time equal to zero and the normalizing time is the natural period. A similar curve is presented in Fig. 9 for the heave motion; however, the beginning portion of the data from the hydraulic study appeared to be influenced by the release of the buoy model at the start of testing. Thus the curve for the hydraulic model was arbitrarily shifted to the left so that the subsequent vibration would be in phase with those from the numerical work.

One minor but interesting phase of this work was to observe the predicted motion of the buoy on the surface of a wave. For this part of the work it was assumed that the buoy was moored in 200 feet of water with an elastic material that produced an equivalent spring

constant at the buoy of 10 lbs/ft, always directed toward the anchor, with an initial tension of 50,000 lbs. As in all the work involving waves, the wave height is built up linearly with respect to time over one wave period. Thus Fig. 10 shows how the wave height was increased over the first wave period and how the buoy and mooring behaved for a wave 260 feet long and 36 feet high. For this case the mass-spring system in conjunction with the water particle acceleration was such that the attachment point was exposed to the air shortly after 14 seconds and the program was written to stop for such an occurrence. Figure 11 shows the buoy successfully negotiating the same wave for the free-floating condition and Fig. 12 shows successful transit of the moored condition when the wave height was reduced to 30 feet. A much longer and higher wave is presented in Fig. 13. Figure 13 clearly shows the buoy heaving on the wave at the natural damped period of 3.1 seconds, as well as at the period of the wave.

Water Sheave

Another minor but very interesting investigation made during this study was that which is sometimes referred to as the "water sheave" effect. An illustration of the problem is, say, a mooring in 20,000 feet of water subjected to a 150 kt. wind. At some time the wind suddenly shifts 180° and blows the buoy back along the alignment of the mooring line until it and the line reach new equilibrium positions. How the line tension varies during the transient motion has been in question. It is felt that the form of the line tension solution presented here, based on the method of characteristics, is particularly well suited to handle this problem in a numerical manner.

A similar problem as that posed above was investigated. However, in order to save computer time the top of the line was translated at a higher velocity than would be the case if the wind drag only on the buoy were reversed. First it was determined that if the buoy broke free from the mooring, a 150 kt wind would push it through the water with a speed of 15 fps. It was decided to translate the line at the conservatively much higher velocity of 25 fps, increasing it linearly from 0 fps in the period of 20 seconds. An initial "in place" or tensioned slope of about 1.3 was assumed and the initial non-equilibrium tension of 7000 lbs. was established with a line diameter of 1.5 inches for a material with characteristics as shown in Fig. 3. The first computation consisted of fixing the top of the line in place and allowing it to reach an equilibrium position. Both positions are shown at time equal to zero on Fig. 14. Then the line was moved to the left with the velocity function presented above. The sequential positions of the line as determined by the numerical computations are shown in Fig. 14.

The tension in the line dropped during the first 150 seconds and then gradually increased until nearly rupturing the line, at which time the computations were stopped. During the increase in tension phase the maximum tension occurred at about 0.967 the distance down the line. The line length changed in accordance with the state of tension along the line. The tension contours on the s-t plane are shown in Fig. 15. It should be noted when examining Fig. 15 that station 1 represents the anchor and subsequent station numbers are spaced 866.7 feet apart. It can be seen that the tension at the anchor decreased for about the first 150 seconds and then steadily

increased. Toward the end of the computations the tension in the line was nearly constant with respect to line position, which is reasonable by inspection of Fig. 14.

If the top boundary condition had been the actual buoy with the wind only driving it, the tensions would have been lower because of the lower buoy velocity and because of the differences in the initial loading condition. When the horizontal component of the line tension at the buoy had equaled the wind drag of 10,800 pounds the buoy-motion would stop. Thus it can be seen that the conditions imposed were much more severe than what would have been experienced at sea. If the submerged weight of the anchor were less than about 10,000 pounds it would have been lifted from the bottom (assuming no adhesion to the bottom) at around 1000 seconds or more. If the real boundary condition had been imposed at the buoy end, the motion would have been quite slow and the computer time necessary to complete the problem would have been prohibitive within the budget for this study.

Effects From the Environment at Sea

The main purpose of this research was two-fold; 1.) to complete the debugging of the numerical program and to test it against closed mathematical solutions, as already discussed, and 2.) to gain some insight into the influence on dynamic line tensions from different wind and current loads and different line scopes. The work related to the first item has been presented. For the second purpose it was decided to design a few moorings in 20,000 feet of water for certain scopes for a maximum wind condition of 150 kts., subjecting each mooring to waves of various frequencies. Then the same moorings were tested with the same waves but with a moderate wind velocity of 50 kts.

The current velocity profiles corresponding to the two wind velocities are presented in Fig. 2.

As presented previously, the computer program first determined the steady state, or equilibrium, position of the lines. The five different conditions are shown in Fig. 16. In all cases the equilibrium tension in the line was kept below 47% of the breaking strength as predicted by Fig. 3. Thus three diameters were selected, as shown in Fig. 16. A summary of the load and scope conditions is given in Table 3.

Two short runs were made in shallow water in order to obtain a brief view of the influence of fairly large waves on line tension. The steady load conditions for these two runs are summarized in Table 3. The profile equilibrium positions have not been included in a Figure because they were practically straight lines.

The dynamic program based on the method of characteristics was compared to the steady state program in terms of the static loads. The procedure was to assume a water depth of 10,100 feet, a scope of 2.02, diameter of 3 inches, a 100 kt. wind, no wave and a surface current of 6 kts. As before, the steady state program determined the equilibrium conditions, which established the initial conditions for the dynamic program. The dynamic program was then allowed to run to a real time of 65 seconds during which no environmental conditions were changed. The configuration of the line changed somewhat, but not beyond what was felt were acceptable limits. It was found that the angle at the top of the line decreased (which was anticipated because of the change from equal angle increments to equal distance increments along the line) as well as the angle at the bottom of the line. The

program ran until the angle at the top decreased to a minimum value, and then was increasing to when the computations were stopped. The line tensions were re-distributed somewhat but the total line length and the buoy coordinates changed very little. A summary of the computations is given in Table 5.

It was next desired to subject the five mooring conditions to waves of various frequencies, or lengths. In each case the wave height to length ratio was kept constant at 1:15. Thus the waves were not nearly breaking but also they could not be classified as small amplitude waves. The dynamic tensions at various stations along the line were determined and plotted by the computer. Generally, the maximum dynamic tensions occurred at the buoy or at the anchor. Examples of tensions at the buoy and at the anchor are presented as Figs. 17 through 32. Point 31A refers to the attachment point at the buoy. It will be noticed that other frequencies, in addition to the frequency of the imposed wave, are present. All periods of frequencies in evidence will be accounted for later.

The computer output included tension contours in the s - t plane. Examples are shown for conditions I through V for the 500 feet long wave as Figs. 33 through 37. The value of each contour line has not been indicated but can be determined by the reader by referring to Figs. 17 through 32. The important thing in Figs. 33 through 37 is to notice the pattern of line tensions. The nodes of zero or small tension fluctuations are clearly visible, as are the regions of maximum tension fluctuations. Equations 33 or 49 can also be used to approximate the locations of the nodes if the z is replaced with s . That is, the nodes occur where $\cos \omega s/a = 0$. A comparison of the

results obtained from the numerical model with those from Eqs. 33 and 49 is presented in Table 6. The comparison is fairly good except at the highest wave frequencies. Thus the position of the nodes can be estimated from Eq. 33, regardless of the line curvature. This introduces the possibility of determining the best position for locating sensitive instrumentation, at least with respect to line position. That is, the positions of minimum displacement variation can be determined from Eqs. 31 and 44 by setting $\sin \frac{\omega S}{a} = 0$, or the minimum tension variation can be determined by setting $\cos \frac{\omega S}{a} = 0$ or the minimum line velocities can be determined from a contour map of velocities or by taking the total time derivatives of Eq. 31 or 44.

A complete summary of the runs made with waves for conditions I through V is given in Tables 7 through 11. Included in the Tables is the value of the damping coefficient, Q , used, the range, or double amplitude, of dynamic tension, the mean value of line tensions at the end of the run, the periods of the frequencies evident in the output records and a calculated line tension based on Eq. 33 for which the length of the line was taken as the "stretched" or "in-place" length at time equal to zero, and the modulus of elasticity was taken as that corresponding to the tension in the top of the line at time equal to zero.

It is desirable to be able to display and compare mooring line tensions in a way that takes into account the difference in line diameter and length, the differences in wave height and frequency and the resonant frequencies. Thus it is desirable to normalize the tensions and corresponding frequencies to compare the results of different types of moorings. The normalizing factor for tensions for

this study was based on the total saturated mass of the line (excluding the added mass) and a characteristic wave acceleration. Thus

$$\text{Normalizing force} = \mu L H \omega^2 \quad (50)$$

Since eq. 33 can predict the nodes in the line fairly well for the moorings presented here, it was felt that Eq. 34 may suffice for predicting, at least approximately, the resonant frequencies with regard to line tensions despite the presence of considerable curvature in the line. Thus the first modal frequency predicted by Eq. 34 was used as the normalizing frequency. Conveniently, the first resonant condition should occur at $f/f_1 = 1.0$ and the subsequent higher mode resonant conditions occur at $f/f_1 = 2.0, 3.0, 4.0$, etc. The resonant frequencies of interest for the five conditions are presented in Table 12. The resulting normalized frequency response curves for conditions I through V are presented as Fig. 38 for mooring line tension at the buoy and Fig. 39 for mooring line tension at the anchor. Admittedly, the data is sparse, but the trend for moorings considered here is clear. That is, the greatest dynamic response, especially at the resonant conditions, occurs for the higher wind conditions. The next most influential parameter is the line scope. It has already been seen, and is common knowledge, that scope is a most important parameter for steady state loads. The responses at higher frequencies tend to be damped out due to hydrodynamic action. No data was obtained for $f/f_n = 1.0$ because such a condition would be due to waves considerably longer than 1000 feet and such long waves were uneconomical to consider. However, little energy exists for waves longer than 1500 to 2000 feet in most wave spectra.

With several curves like Figs. 38 and 39 for a complete range of water depths, scopes, line diameters and types, it may be possible to generate a non-dimensional empirical solution for dynamic line tensions for any homogeneous one point mooring. Or perhaps analytical transfer functions based on linear systems, which are being developed by others, can be compared to results like Figs. 38 and 39, which consider most of the non-linearities in the problem. This subject has been left for future study.

In order to test the program for quite shallow water conditions and to gain whatever information possible with just two runs, condition VI for a depth of 150 feet and condition VII for a depth of 1000 feet were investigated for a wave 600 feet long and 40 feet high.

For the depth of 150 feet the sequential positions of the line are shown in Fig. 40 from time zero to 13 seconds. At about time equal to 14 seconds the line tension became negative and the program stopped because a square root of the negative tension occurs. The line tension, which was nearly constant along the line at any time is shown in Fig. 41.

For the depth of 1000 feet the line remained nearly straight for all motion. The line tensions again were nearly constant along the line at any time. The fluctuations in the tension at the buoy and at the anchor are shown in Fig. 42. It should be recalled for both conditions VI and VII that the wind velocity was 50 kts.

SUMMARY AND CONSLUTIONS

A review of the basic equations for the numerical modeling of the mooring line motion based on the method of characteristics and the motion of the buoy has been made. Solutions for a homogeneous mooring line have been presented which include hysteretic damping and hydrodynamic damping. In addition, a summary of analytical solutions for a straight, taut mooring line has been presented and it was attempted to apply the procedures developed to the single point curved, or less taut, moorings. It was found that this approximate procedure did poorly for estimating mooring line tension but did quite well in estimating the positions of the nodes of tension and in predicting the natural resonant frequencies of the line.

A new way of presenting frequency response curves for taut or slack mooring lines subjected to waves was suggested. The normalizing procedure makes it possible to show the frequency response for lines of different lengths, diameters and materials on the same scale. Thus the influence of scope and wind magnitude on dynamic mooring line tension was presented while normalizing the influence of line diameter. It was found that smaller scope and/or higher wind increased the dynamic tensions drastically, as well as the steady state, or mean line tension.

Two runs were presented for shallow water. It was seen that a large wave in 150 feet of water would have been disastrous to a 2 inch diameter line. However, the same wave in 1000 feet of water with the same line and scope produced reasonable dynamic tensions. It was seen that the tension was nearly constant along the line at any time.

Probably a static solution approach would be adequate wherein the line tension would be determined based on the sequential positions of the buoy on the wave and the subsequent change in scope without regard to accelerations. However, this procedure would be very inadequate for deep water moorings.

A presentation of the water sheave problem was made which illustrated an additional application for the numerical program.

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TABLES

TABLE 1. - COMPARISON BETWEEN THEORY AND THE NUMERICAL MODEL FOR LONGITUDINAL DYNAMIC TENSIONS IN A STRAIGHT LINE.

Depth or Line Length (ft.)	Variation in Line Tension at the Anchor (lbs)		Variation in Line Tension at the Top of the Line (lbs)	
	Num. Model	Eq. 33	Num. Model	Eq. 33
5,000	1,380	1,330	296	273
10,000	3,250	3,200	2,990	2,940
15,000	1,640	1,600	990	932
20,000	1,700	1,750	1,170	1,172

Line diameter = 1.5 inches

Modulus of Elasticity = 13.1×10^6 psf

Line density = 0.02439 slugs/ft (same as sea water)

Amplitude of forcing motion = 15 ft

Frequency of forcing motion = 0.7 rad/sec

TABLE 2. - COMPARISON BETWEEN NATURALLY DAMPED AND FORCEFULLY DAMPED LONGITUDINAL VIBRATIONS FOR A DEPTH OF 20,000 FEET.

Value of the Damping Coeff., Q	Variation in Line Tension at the Anchor (lbs)		Variation in Line Tension at the top of the Line (lbs)	
	Num. Model	Eq. 33	Num. Model	Eq. 33
0	3,237	∞	3,677	∞
$\frac{4 \times 10^5}{\omega}$	2,085	N.A.	2,348	N.A.

Same line and forcing characteristics as for Table 1, except.

Frequency = 0.6105 rad/sec

TABLE 3. - SUMMARY OF STEADY LOAD CONDITIONS FOR THE FIVE MOORINGS IN
20,000 ft. Time = 0

Condition No.	Wind Vel. (Kts)	Line Dia. (in)	Scope	"Stretched" Scope	Tension at Buoy (lbs) % UIT	Tension at Anchor (lbs) % UIT
I	150	3.0	0.80	1.03	<u>99,804</u> .47	<u>86,614</u> .41
II	150	2.5	0.87	1.11	<u>47,777</u> .44	<u>41,077</u> .38
III	50	2.5	0.87	1.03	<u>16,177</u> .15	<u>9,427</u> .09
IV	150	2.0	1.18	1.50	<u>27,699</u> .40	<u>23,596</u> .34
V	50	2.0	1.16	1.34	<u>6,983</u> .10	<u>2,635</u> .04

Note: Scope = Length of line on land ÷ water depth
 "Stretched" scope = Length of line under load, in place ÷ water
 depth

TABLE 4. - SUMMARY OF STEADY LOAD CONDITIONS FOR THE TWO MOORINGS IN SHALLOW WATER. Time = 0 Wind Velocity = 50 kts

Condition No.	Water Depth (ft)	Line Dia. (ins)	Scope	"Stretched" Scope	Tension at Buoy (lbs) $\frac{1}{4}UH$	Tension at Anchor (lbs) $\frac{1}{4}UH$
VI	150	2	1.32	1.50	$\frac{2,021}{.03}$	$\frac{2,001}{.03}$
VII	1,000	2	1.32	1.50	$\frac{2,564}{.04}$	$\frac{2,394}{.03}$

TABLE 5. - COMPARISON OF EQUILIBRIUM CONDITIONS BETWEEN THE STEADY STATE PROGRAM AND THE DYNAMIC PROGRAM

Program	Time (secs)	Angle at Buoy (Rad)	Angle at Anchor (Rad)	Tension at Buoy (lbs)	Tension at Anchor (lbs)	Total Line Length (ft)	X-Coordinate of Buoy (ft)
Steady State	0	1.089	0.097	19,977	15,383	24,327	21,531
Dynamic	65	0.902	0.021	21,817	12,141	24,252	21,320
<u>Steady</u> <u>Dynamic</u>		1.21	4.66	0.915	1.265	1.002	1.010

TABLE 6. - COMPARISON OF TENSION NODES BETWEEN THE NUMERICAL MODEL AND EQ. 33

Condition	Wave Length (ft)	Node Position from Numerical Model (ft)	Node Position from Eq. 33 (ft)	
I	500	4,800	6,920	
		18,200	20,600 (at buoy)	
II	145	4,440	3,680	
		11,600	11,000	
		18,900	18,400	
	325	5,900	5,500	
		17,000	16,500	
	500	6,240	6,800	
		19,500	20,400	
	1,000	10,600	9,650	
	III	145	4,800 ?	7,400
			10,300 ?	12,300
14,400 ?			17,200	
325		3,910	3,690	
		11,700	11,100	
500		5,150	5,150	
		15,100	15,400	
630		5,500	4,600	
		16,000	13,800	
1,000		7,550	6,450	
	18,700	19,300		

TABLE 6. - Continued

Condition	Wave Length (ft)	Node Position from Numerical model (ft)	Node Position from Eq. 33 (ft)
IV	150	4,020	3,730
			11,200
		17,250	18,700
	275	7,030	5,050
		17,400	15,200
	500	8,003	6,800
		21,600	23,400
	600	8,350	7,450
		23,300	22,300
V	150		2,510
		9,800	7,550
			12,500
	275		3,400
		9,700	10,200
	460	4,450 ?	4,360
			13,100
	500	4,450	4,580
			13,700
	600	4,450	5,000
		10,500 ?	15,000

TABLE 6. - Continued

Condition	Wave Length (ft)	Node Position from Numerical model (ft)	Node Position from Eq. 33 (ft)
IV	150	4,020	3,730
			11,200
		17,250	18,700
	275	7,030	5,050
		17,400	15,200
	500	8,003	6,800
		21,600	20,400
	600	8,350	7,450
		23,300	22,300
	V		2,510
		9,800	7,550
			12,500
			3,400
		9,700	10,200
		4,450 ?	4,360
			13,100
		500	4,580
			13,700
		600	5,000
		10,500 ?	15,000

Items in Table:

Dynamic Tension Range	Range From Eq. 55
Mean Tension	Periods

TABLE 7. - LINE TENSIONS AND PERIODS FROM WIND AND WAVE EXCITATION FOR CONDITION I

Wave Hgt. (ft)	Wave Length (ft)	Wave Period (sec)	Damping Coef. Q^{-1} $\left(\frac{\text{lbs}}{\text{ft}^2}\right)$	Conditions at			
				Buoy		Anchor	
33.3	500	9.88	4×10^5	6500	162	5100	12000
				97750	4.9	91950	89300
						4.9	9.8

Items in Table:		
Dynamic Tension Range	Dynamic Tension Range	From Eq. 33
Mean Tension	Mean Tension	Periods

TABLE 9. - LINE TENSIONS AND PERIODS FROM WIND AND WAV' EXCITATION FOR CONDITION III

Wave Base ht. Length (ft)	Wave Period (sec)	Damping Coef. Q^{-1} ($\frac{lbs}{ft}$)	Conditions at									
			Buoy		20		15		10		6	
			24 for 145 and 325 28 for 500 22 for 1000									
9.7 145	5.52	4×10^5	1900 1790	1100	800	600	350	2080	11070	5.2/22	10325	5.1/22
			14750 5.4/22	13800	13300 5.3/22	11700	11070	650	10325	5.1/22	2520	7.9
21.7 325	7.96	4×10^5	2600 1975	2500	2000	2000	2000	2520	11900	8.0	10650	7.9
			15000 7.9	13950	13400 7.8	11900	11900	2520	11900	8.0	10650	7.9
33.5 500	9.88	4×10^5	3500 1920	4000	1550	1800	1800	2740	12100	9.8	10600	9.7
			14850 9.8	14600	13350 9.8	12100	12100	2740	12100	9.8	10600	9.7
40.0 630	11.09	4×10^5	8500		5400	2300	7000		2300		7000	
			15250 11.2		13500 11.0	12500	11000		12500	11.1	11000	11.1
66.7 1000	15.97	2×10^5	2200 1000	4400	4850	950	4600		950		4600	
			15400 7.0/14	13450	13580 14.0	12120	11600		12120	7.0/14.1	11600	7.0/14.1

TABLE 10. - LINE TENSIONS AND PERIODS "RO" WIND AND WAVE EXCITATION FOR CONDITION IV

Wave Length (ft)	Wave Period (sec)	Buoy	Conditions at				Tension in Tows	
			14 for 500	16 for 600	10	2	Anchor	Dynamic Range from Eq 33
10.0	5.41	1900	750	550	550	550	550	5.3
		25750	5.3	23840	5.4	23120	23120	5.3
18.3	7.33	3200	2150	1700	1900	1900	1900	7.3
		26100	7.2	24150	7.2	23450	23450	7.3
33.2	9.88	4700	2100	1950	1950	1950	1950	9.8
		26850	9.9	25400	9.9	24250	24250	9.8
40.0	10.82	8400	5200	6900	6400	6400	6400	10.9
		27200	10.9	35950	10.9	24800	24800	10.9

Items in Table:		
Dynamic Tension	Range	Range from Eq. 33
Mean Tension	Periods	

TABLE 11. - LINE TENSIONS AND PERIODS FROM WIND AND WAVE EXCITATION FOR CONDITION V

Wave Length (ft)	Wave Period (sec)	Bumping Coef. $\frac{Q \cdot 2}{ft^2}$	Conditions at				
			Ruoy	28	20	10	Anchor
10 150	5.41	0	2200 655 5800 5.5/30.6	1700 5450 5.6/30.8	900 4700 5.5/31	220 3750 31	700 1210 8150 31.2
18.5 275	7.33	0	1900 5650 5950 7.4/32	1700 5450 7.5/31.6	1800 5000 7.5/31.2	350 3760 7.2/31.5	800 5820 3200 31.6
30.7 460	9.47	0	2900 5950 9.6/32	2100 5950 9.6/31	1600 4800 9.7/32	650 3840 9.7/31	960 3220 9.6/32
33.5 500	9.88	0	2300 6250 6150 10.2/30.3		1150 5020 10/31	500 3950 10/31	1460 6720 3270 10.2/33
40 600	10.82	0	3600 1180 6200 11/33	2200 6100 11/33	1800 5000 11/31	1000 3900 11/31	1100 2370 3350 10.9/31

TABLE 12. - RESONANT FREQUENCIES FOR THE VARIOUS CONDITIONS, BASED ON EQ. 34

Condition	RESONANT FREQUENCIES (cps)					
	f_1	f_2	f_3	f_4	f_5	f_6
I	0.0672	0.134	0.201			
II	0.0624	0.125	0.187			
III	0.045	0.090	0.135	0.180		
IV	0.046	0.092	0.138	0.184		
V	0.0348	0.0696	0.1045	0.122	0.139	0.174

FIGURES

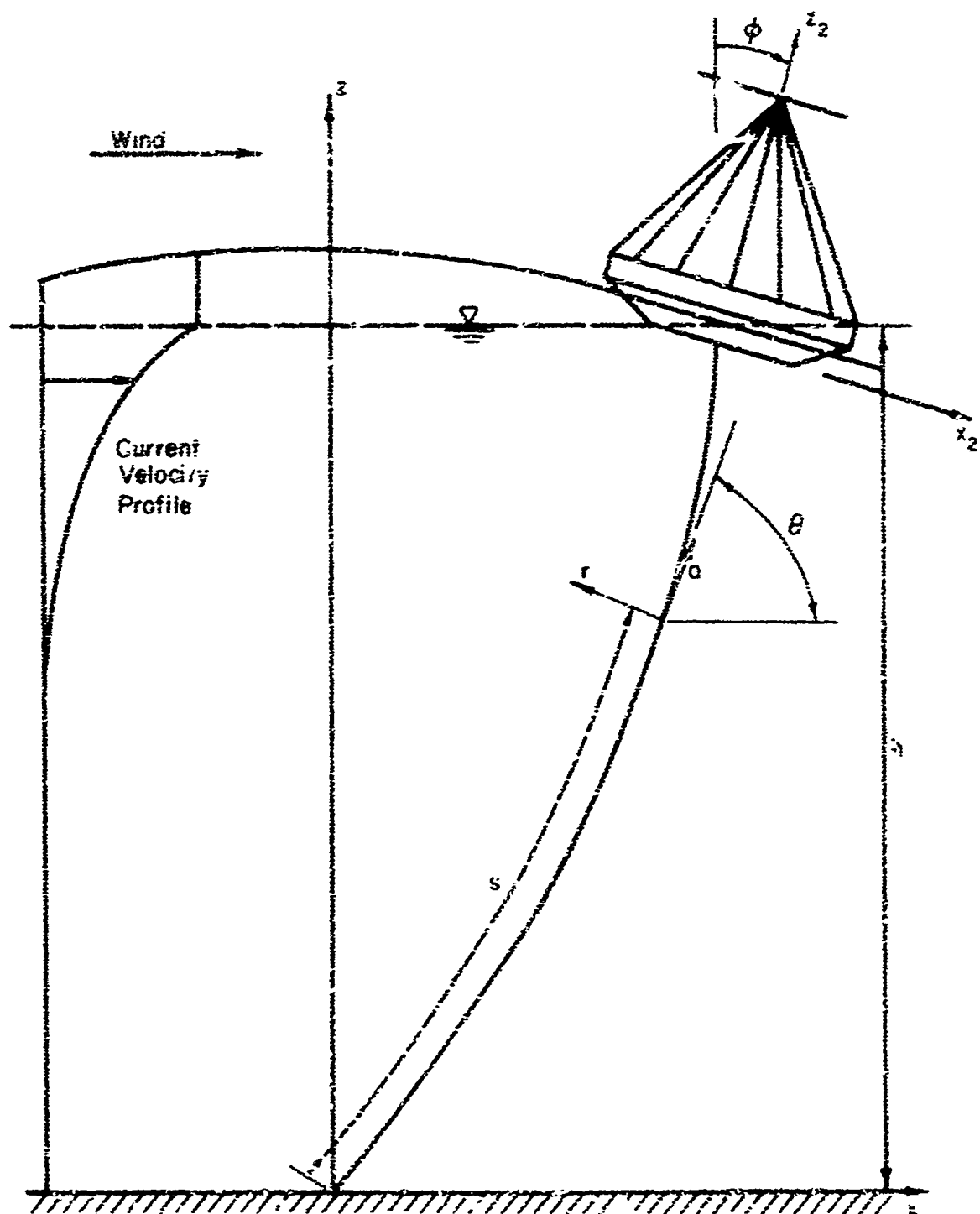


FIG. 1 DEFINITION SKETCH OF THE COORDINATE SYSTEMS.

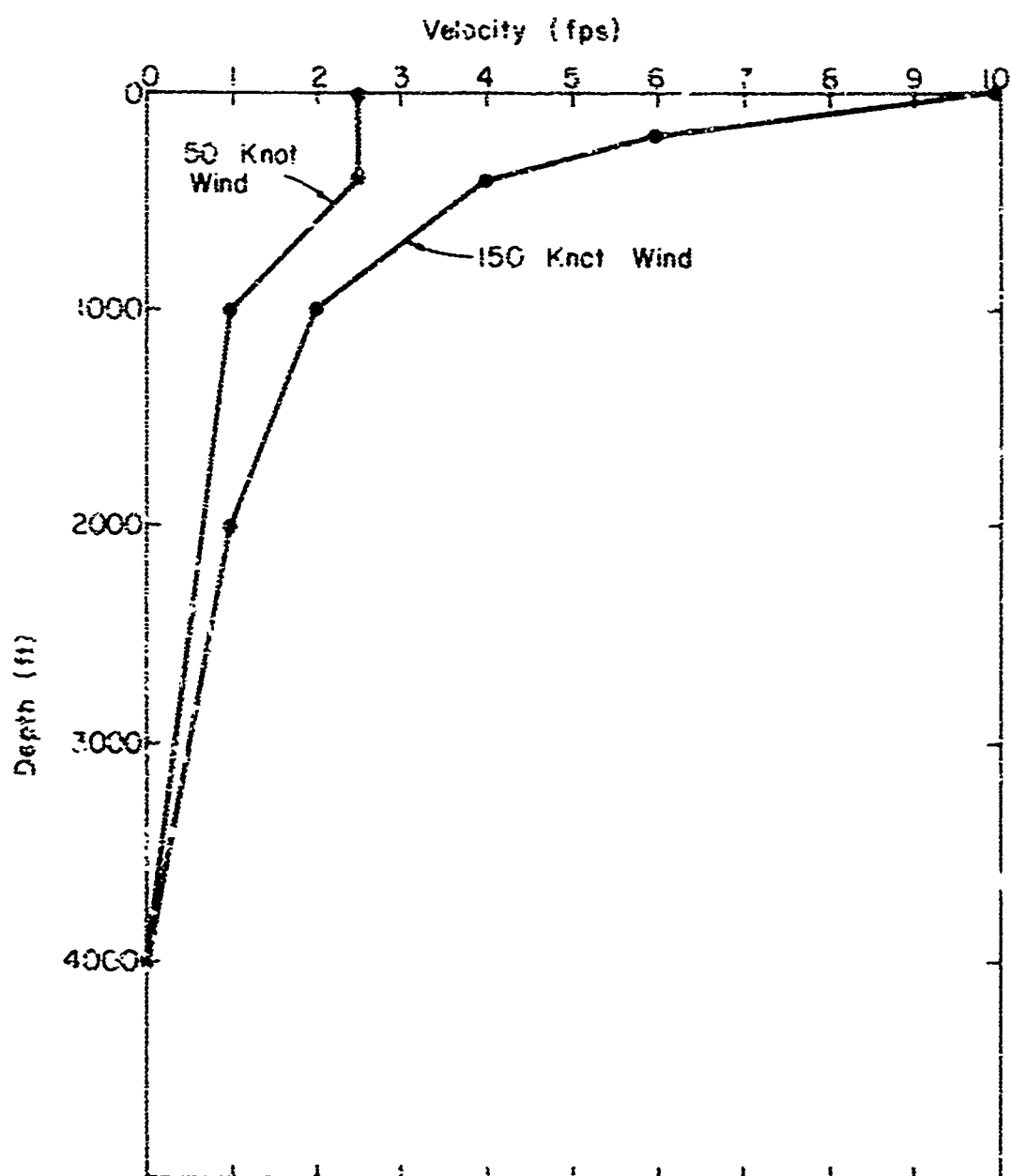


FIG. 2 CURRENT VELOCITY DISTRIBUTION.

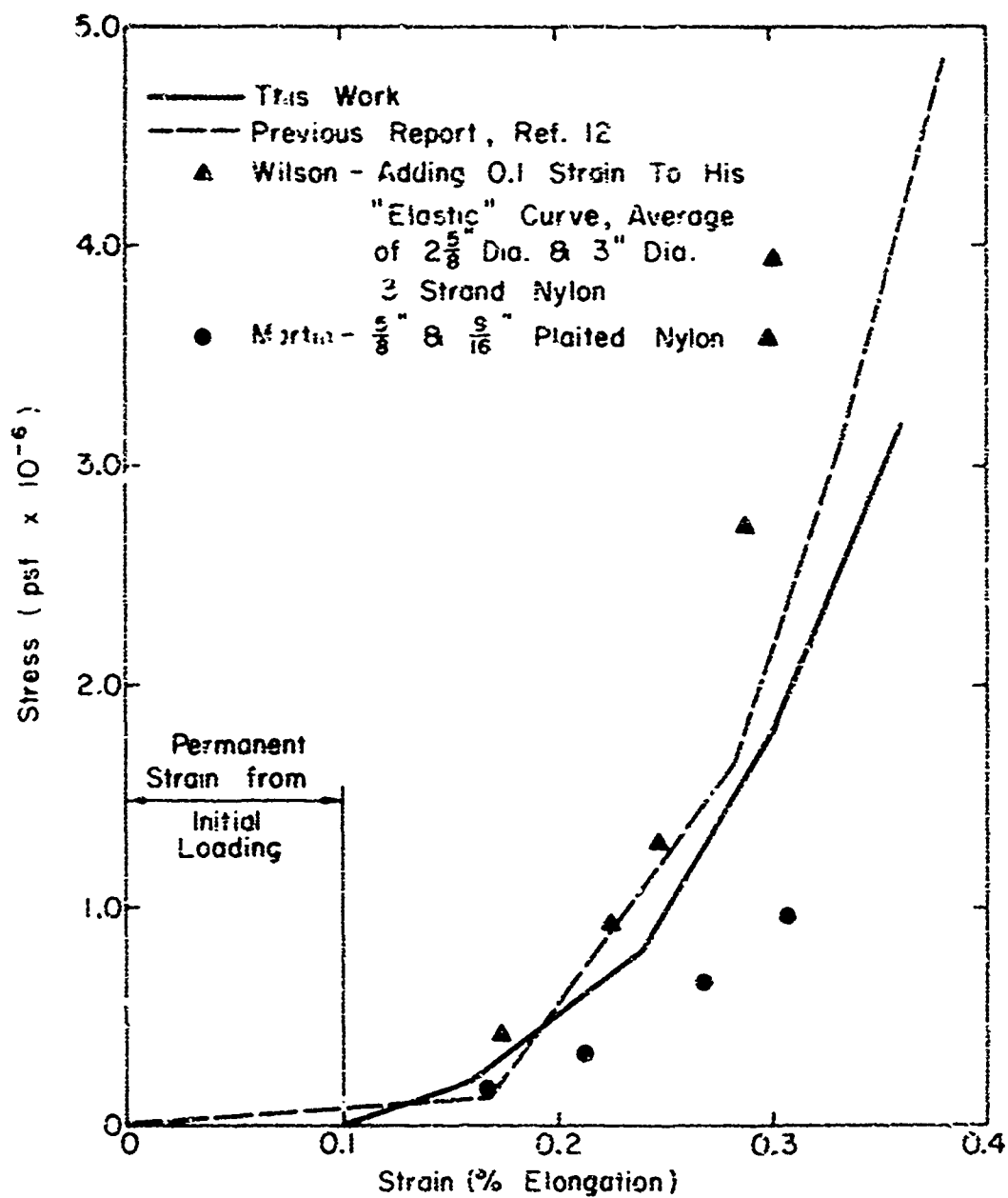


FIG. 3 STRESS-STRAIN DIAGRAM.

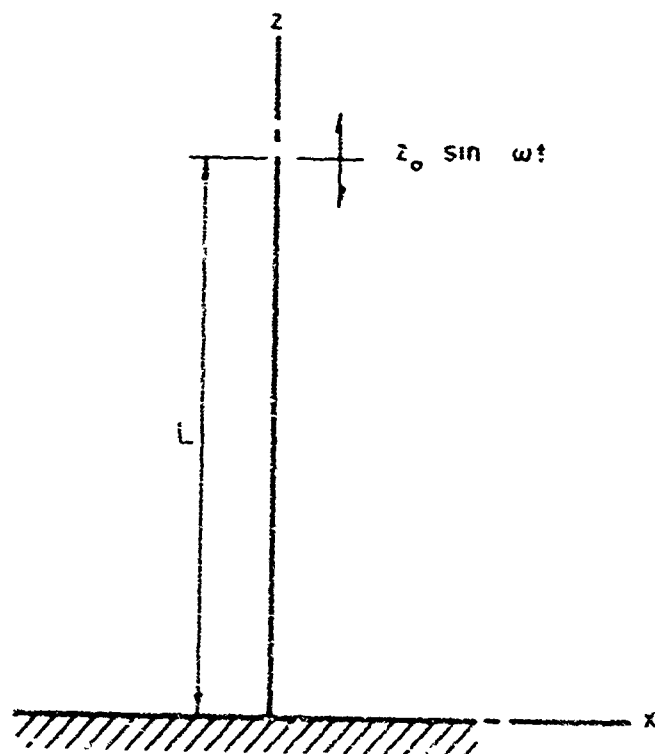


FIG. 4 IDEALIZED VERTICAL LINE.

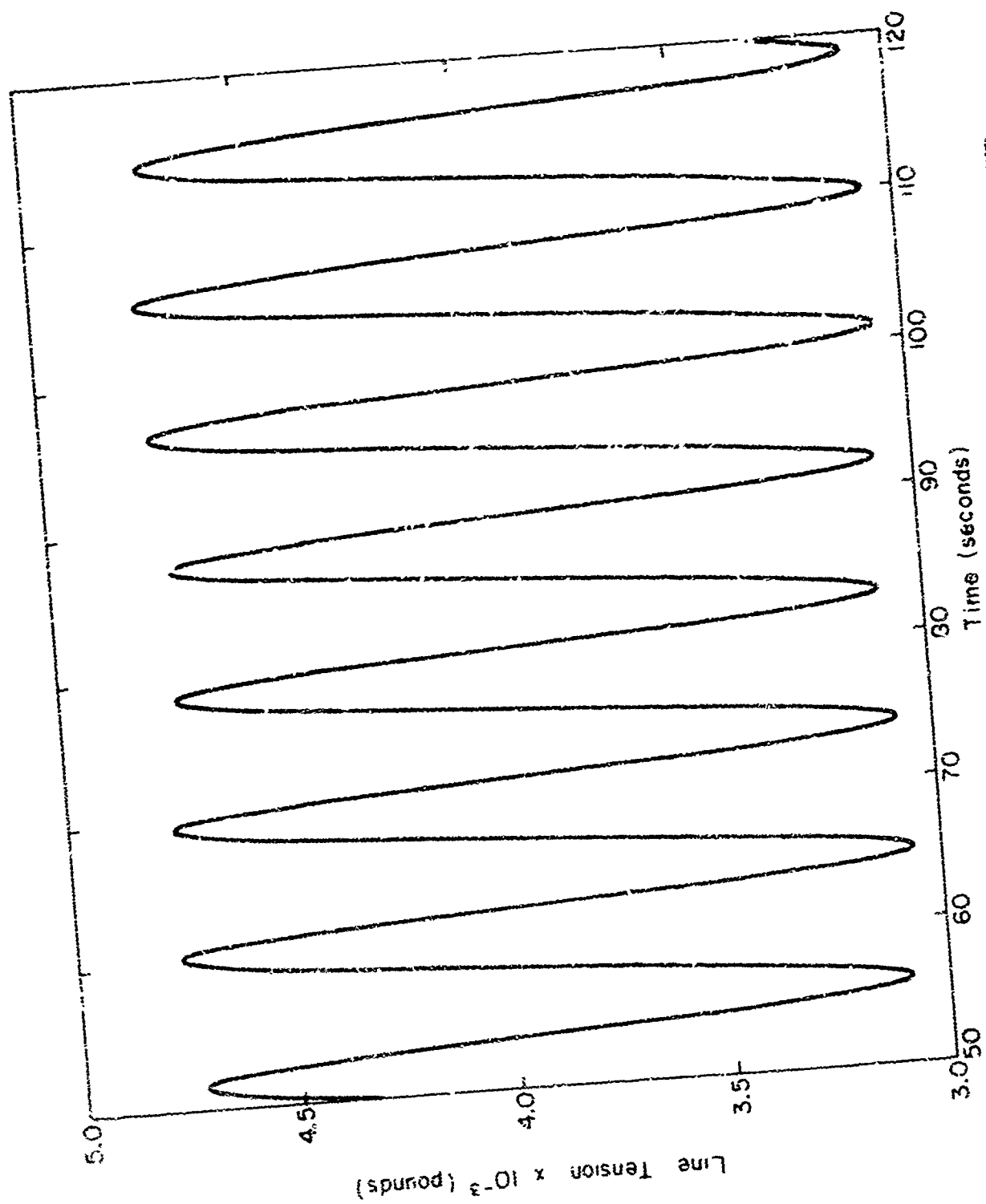


FIG. 5 DYNAMIC LINE TENSION AT THE ANCHOR. WATER DEPTH = 1500 FEET.

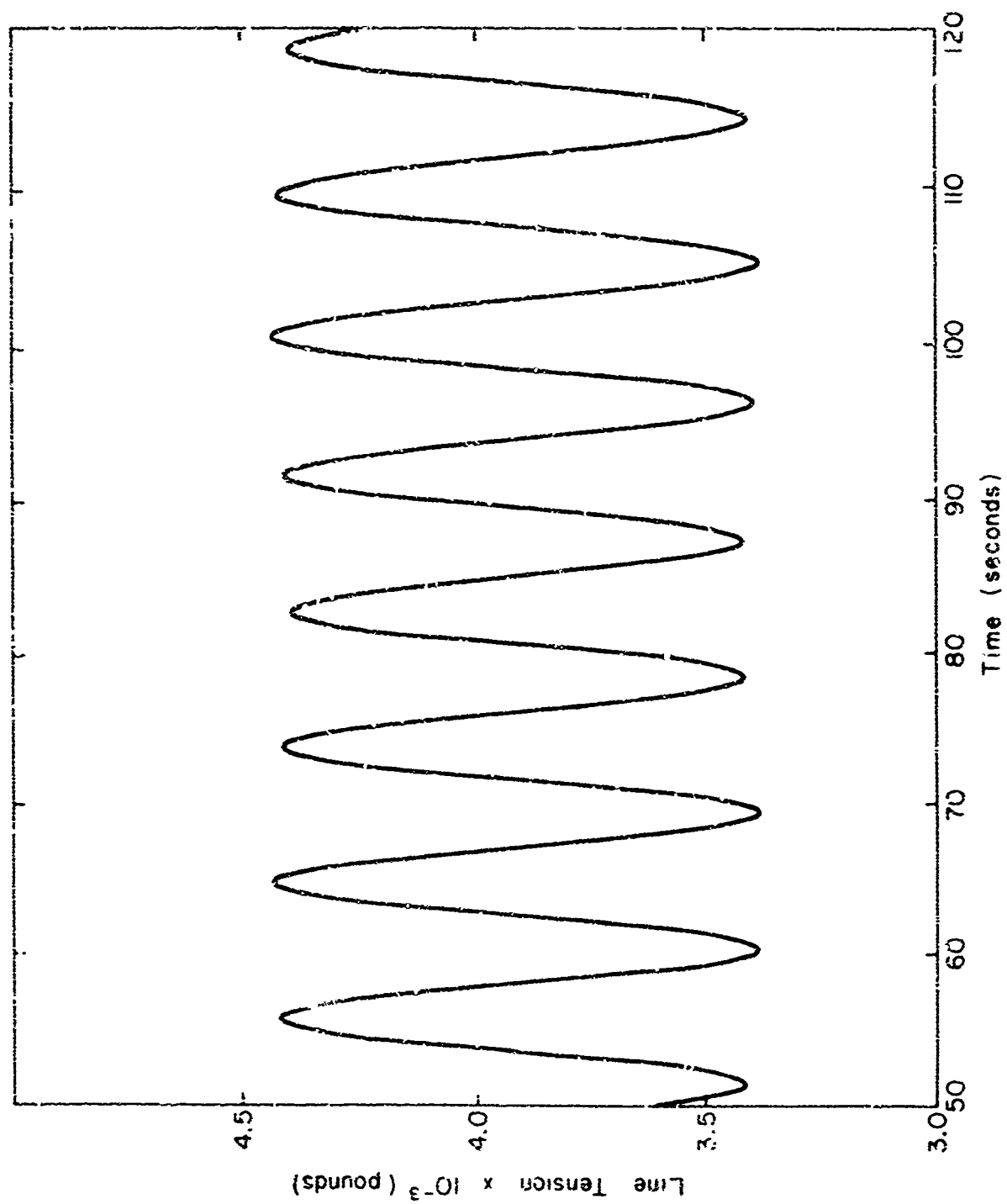


FIG. 6 DYNAMIC LINE TENSION AT THE BUOY. WATER DEPTH = 1500 FEET.

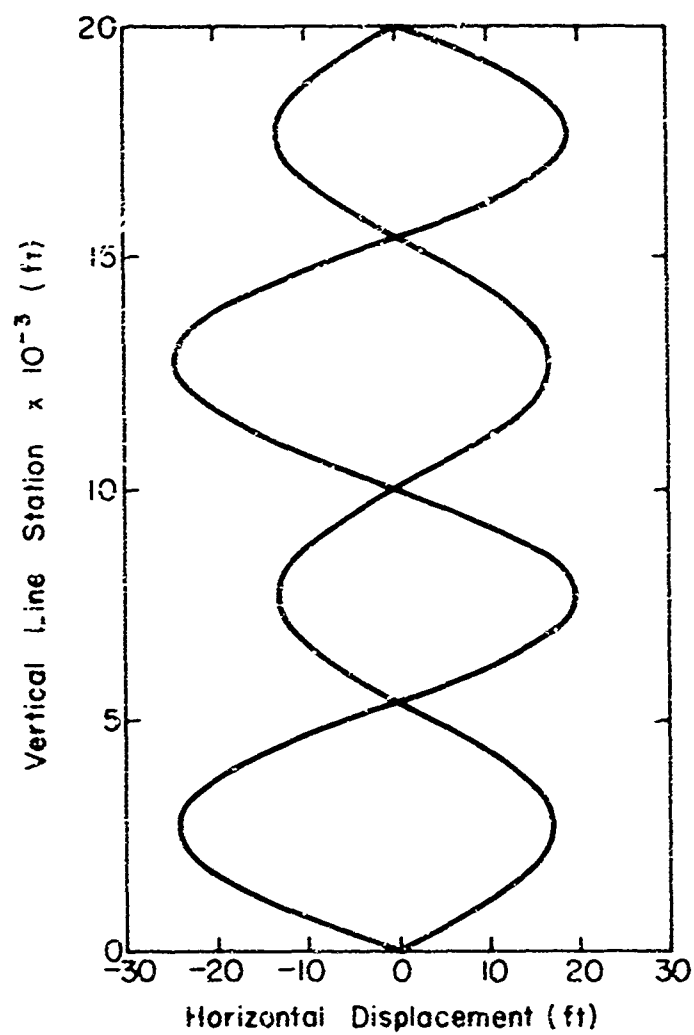


FIG. 7 HORIZONTAL LINE DISPLACEMENT FOR A SINUSOIDALLY DISTRIBUTED INITIAL VELOCITY.

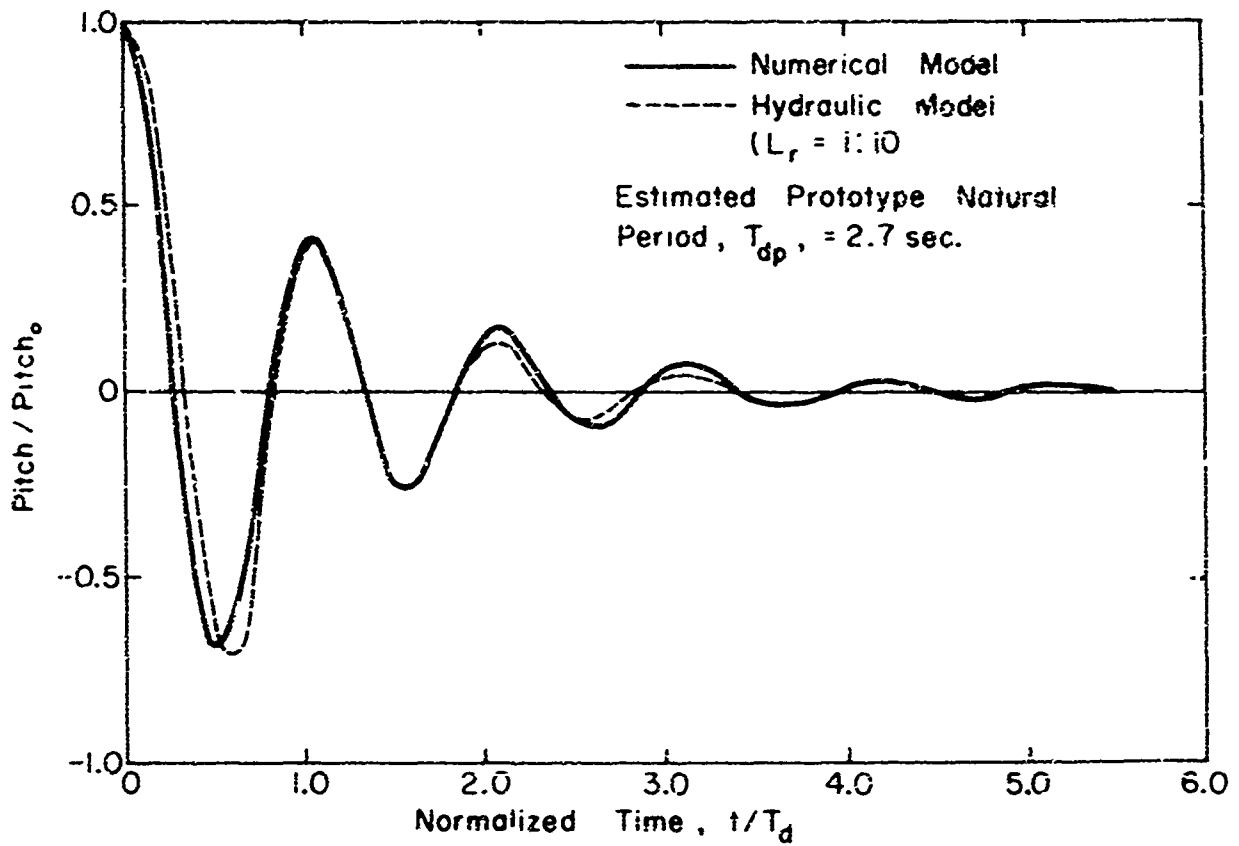


FIG. 8 NORMALIZED PITCH DECAY CURVE.

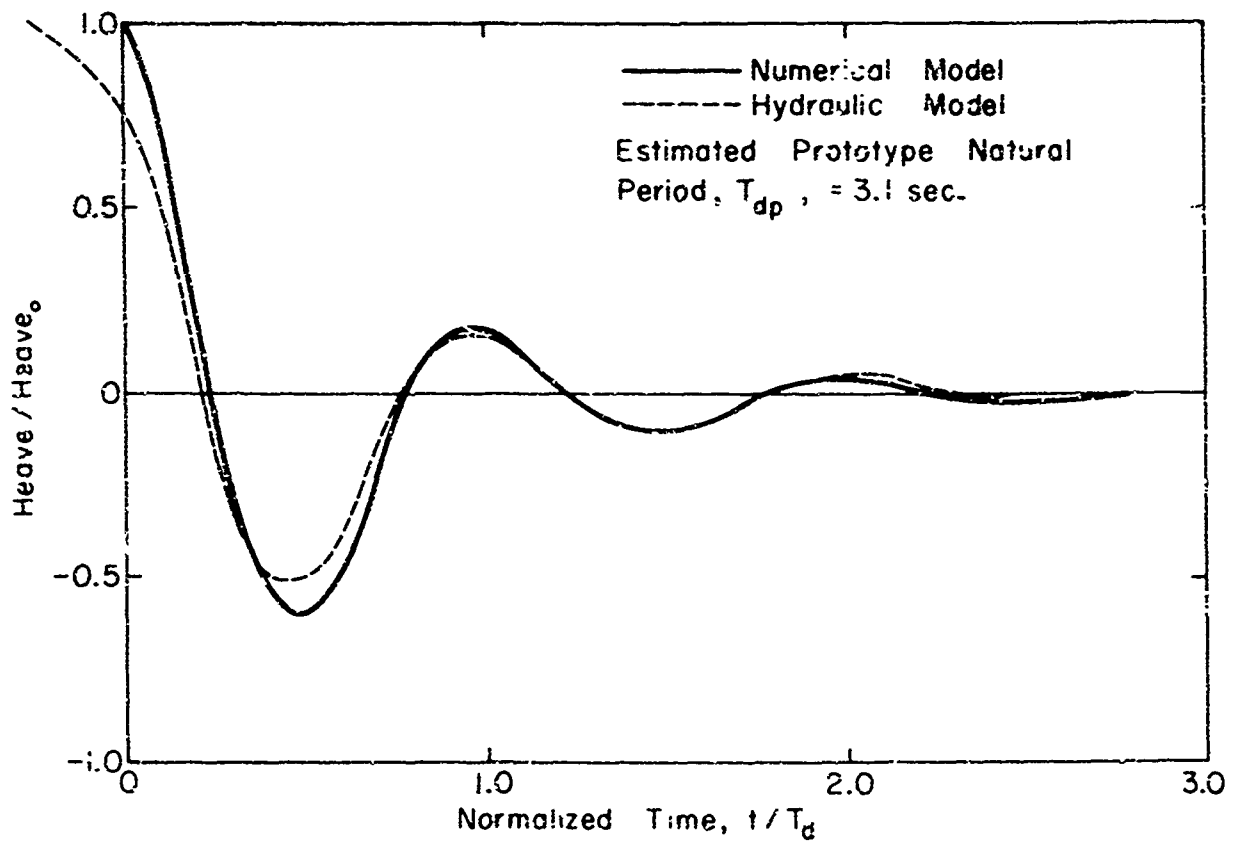


FIG. 9 NORMALIZED HEAVE DECAY CURVE.

Note: Wave Travels From Left To Right. The Relative Positions Of The Buoy With Respect To The Wave Are Shown For Various Times In Seconds.

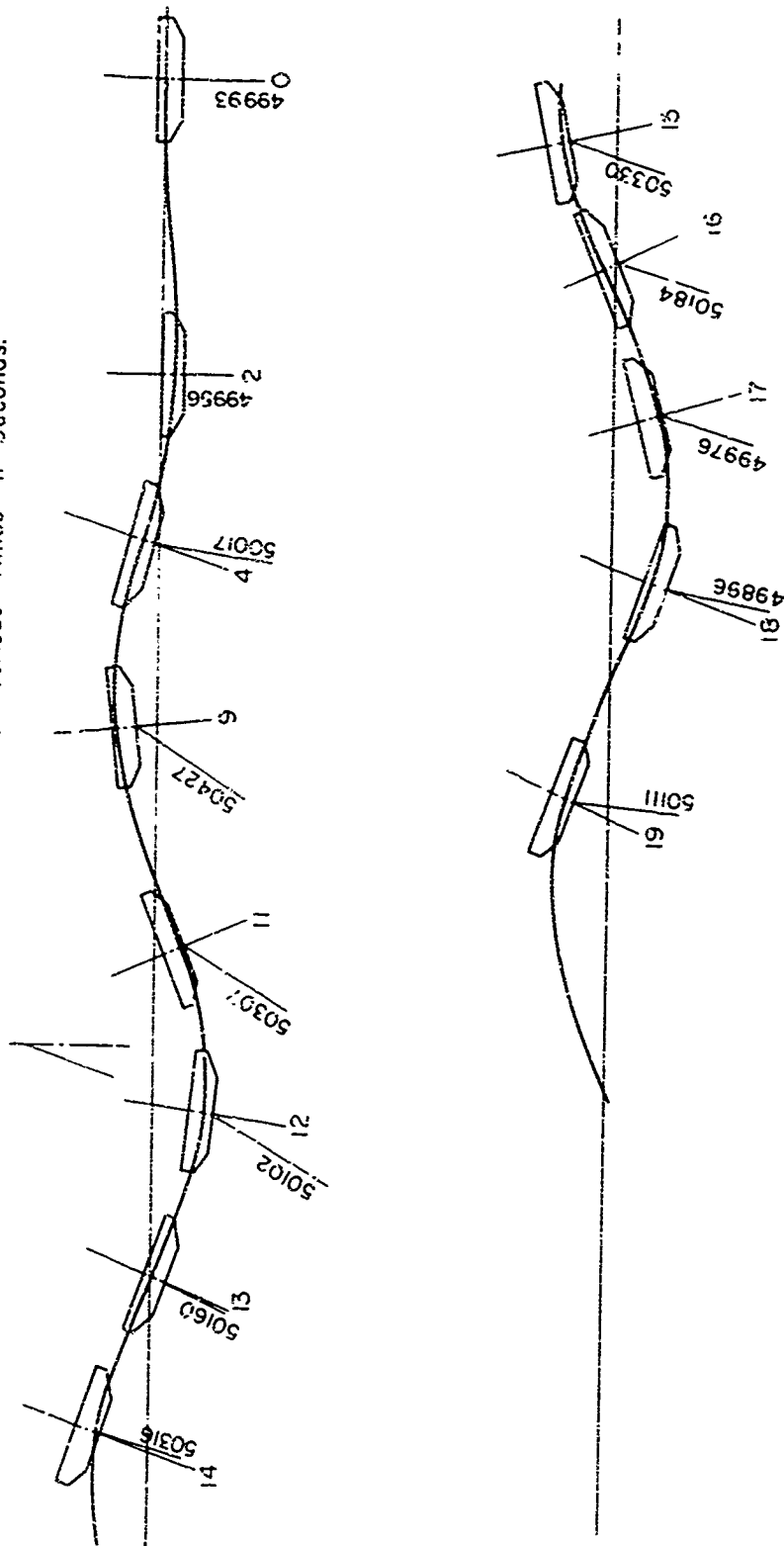


FIG. 10 LARGE DISC BUOY. BEGINNING OF WAVE. ELASTIC MOORING. DEPTH = 200 FT. WAVE LENGTH = 260 FT. WAVE HEIGHT = 36 FT.

See Note on Fig. 10

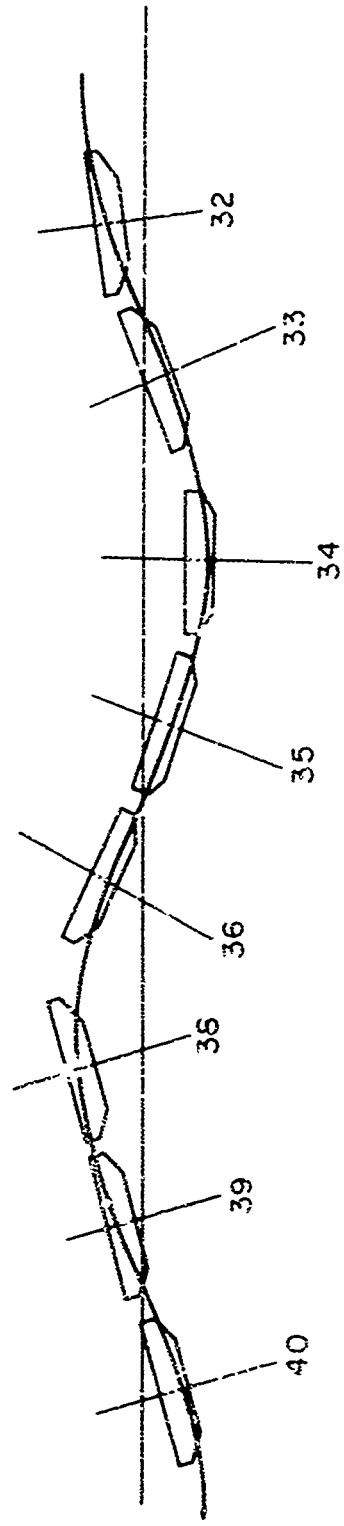


FIG. 11 LARGE DISC BUOY. FREE FLOATING, DEPTH = 200 FT.
WAVE LENGTH = 260 FT. WAVE HEIGHT = 36 FT.

See Note on Fig. 10

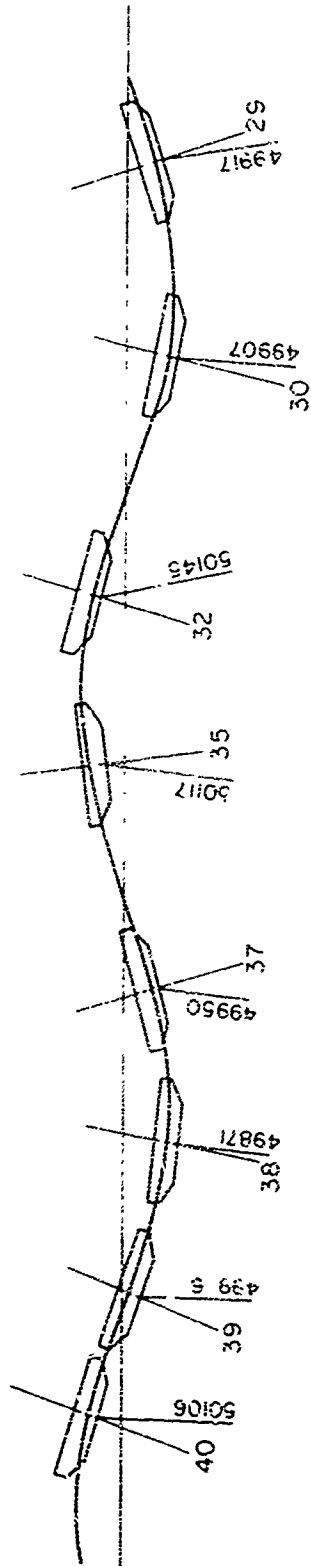
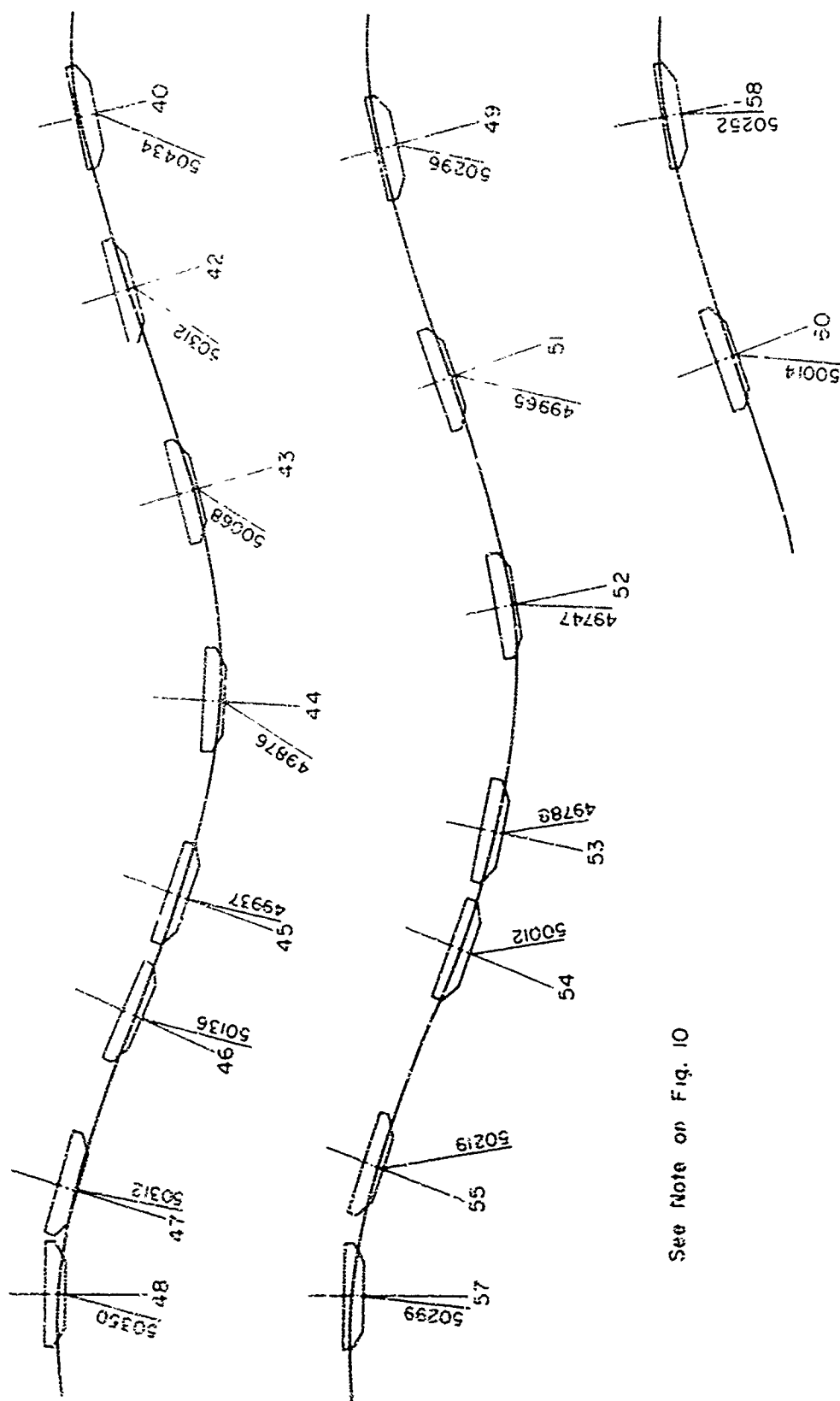


FIG. 12 LARGE DISC BUOY, ELASTIC MOORING. DEPTH = 200 FT.
WAVE LENGTH = 260 FT. WAVE HEIGHT = 30 FT.



See Note on Fig. 10

FIG. 13 LARGE DISC BUOY, ELASTIC MOORING. DEPTH = 200 FT.
WAVE LENGTH = 500 FT. WAVE HEIGHT = 60 FT.

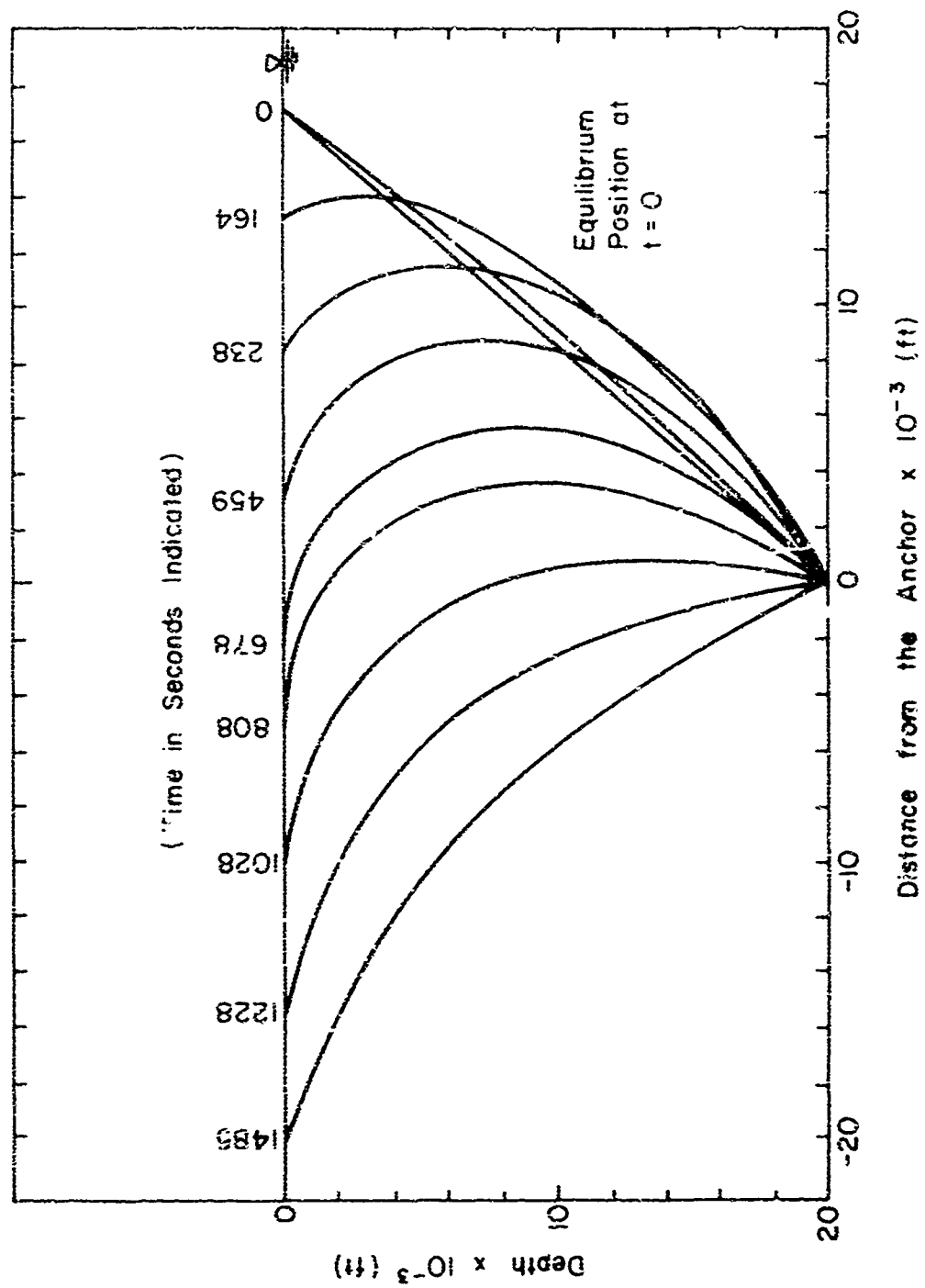


FIG. 14 SEQUENTIAL POSITIONS OF THE 1½ INCH LINE FOR THE WATER SHEAVE PROBLEM.

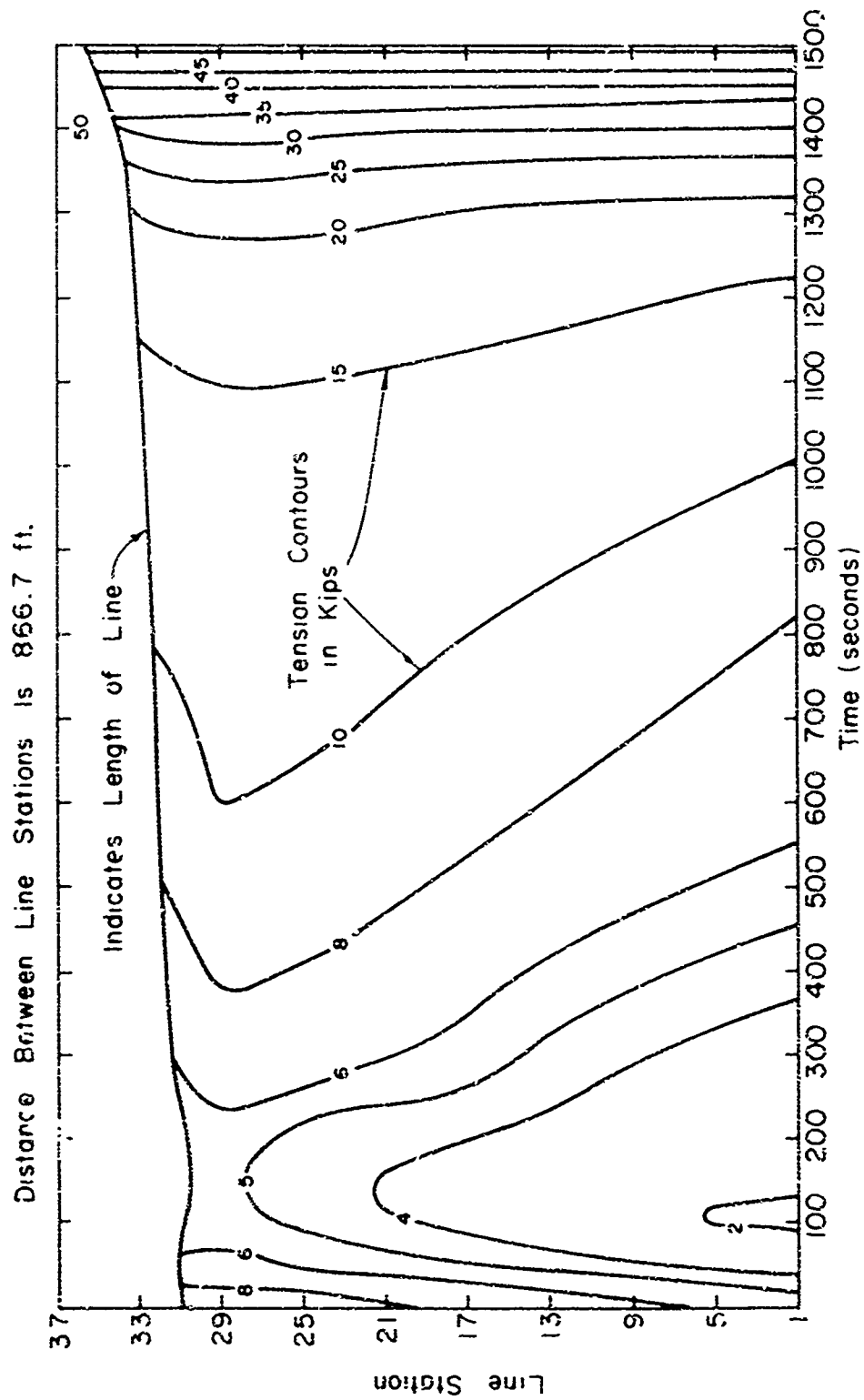


FIG. 15 TENSION CONTOURS IN THE s - t PLANE FOR THE WATER SHEAVE PROBLEM.

- ▲ Cond. I. Scope = 0.80, Wind = 150 kt. Dia. = 3.5 in.
- Cond. II. Scope = 0.87, Wind = 150 kt. Dia. = 2.5 in.
- ◻ Cond. III. Scope = 0.87, Wind = 50 kt. Dia. = 2.5 in.
- △ Cond. IV. Scope = 1.18, Wind = 150 kt. Dia. = 2.0 in.
- Cond. V. Scope = 1.16, Wind = 50 kt. Dia. = 2.0 in.

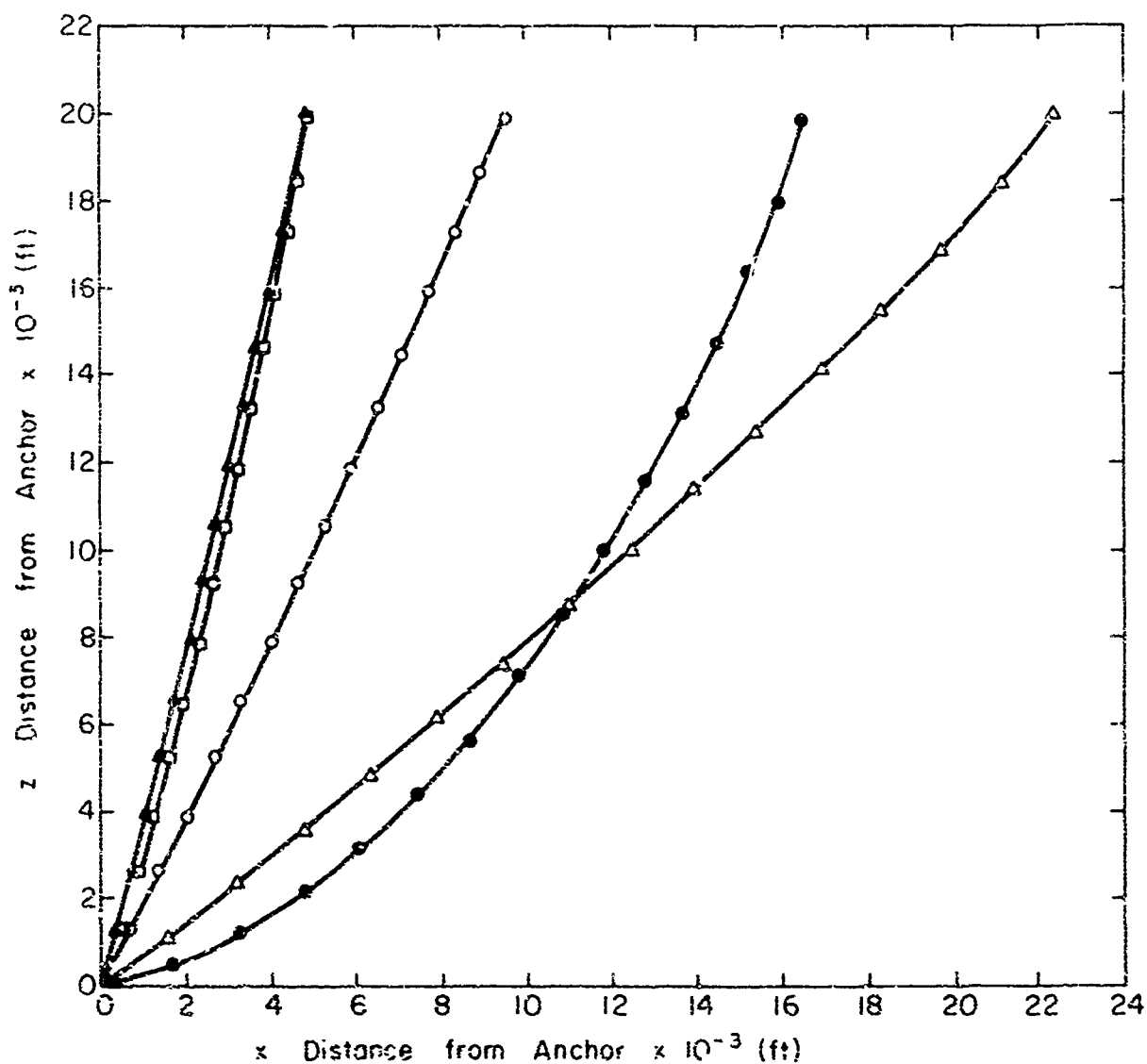


FIG. 16 EQUILIBRIUM POSITIONS FOR VARIOUS MOORING CONDITIONS STUDIED.

POINT 31A

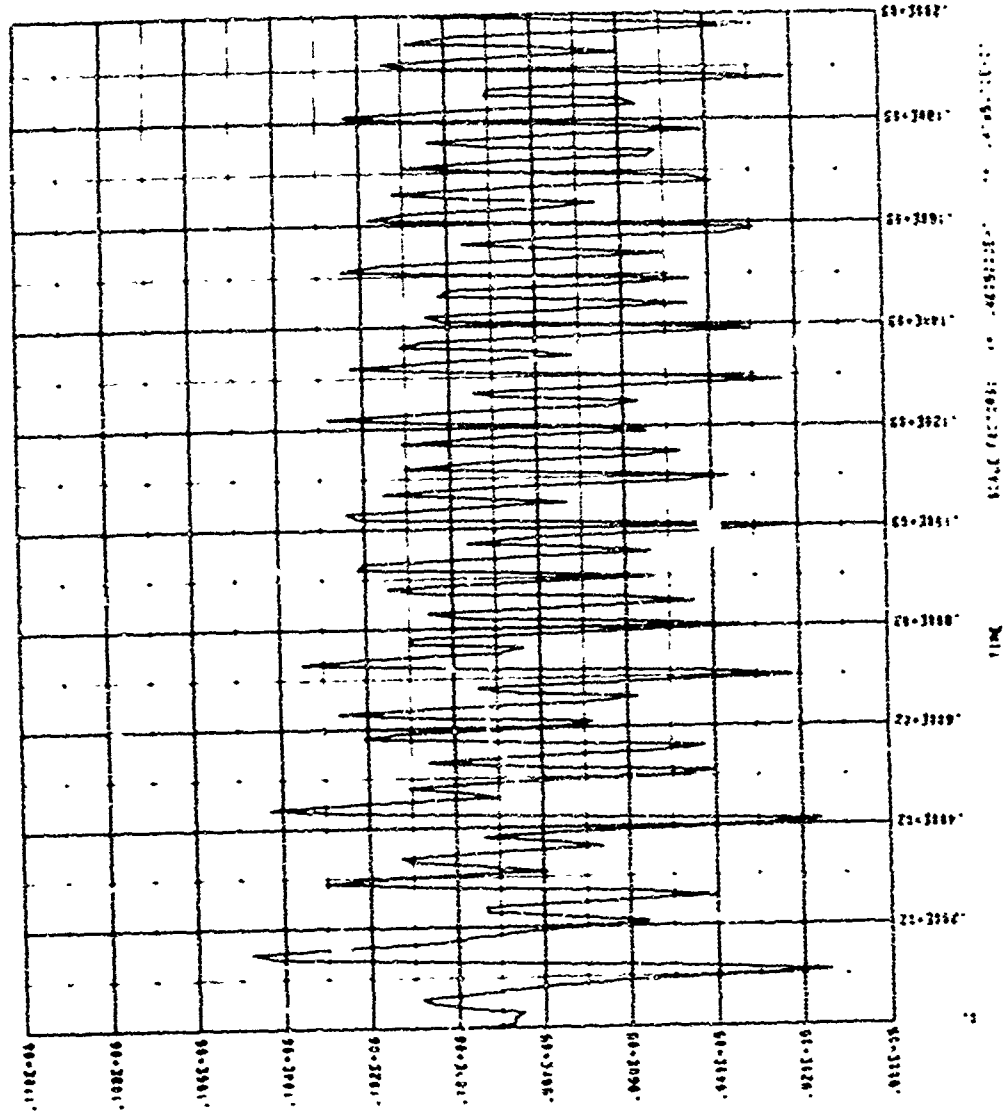


FIG. 17 TENSION AT THE BUOY. CONDITION 1. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

ANCHOR

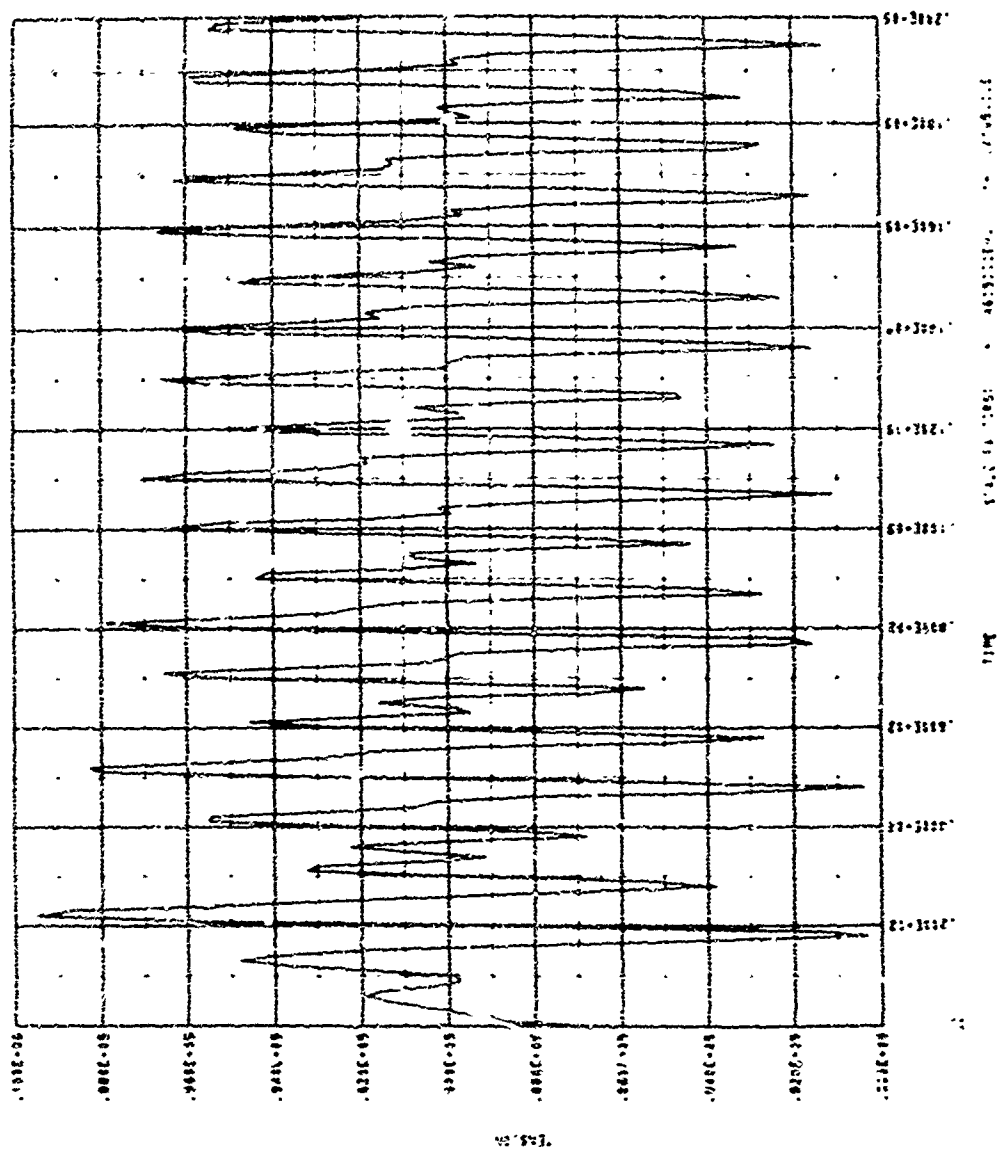


FIG. 18 TENSION AT THE ANCHOR. CONDITION 1. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.5 FT.

POINT 3-1

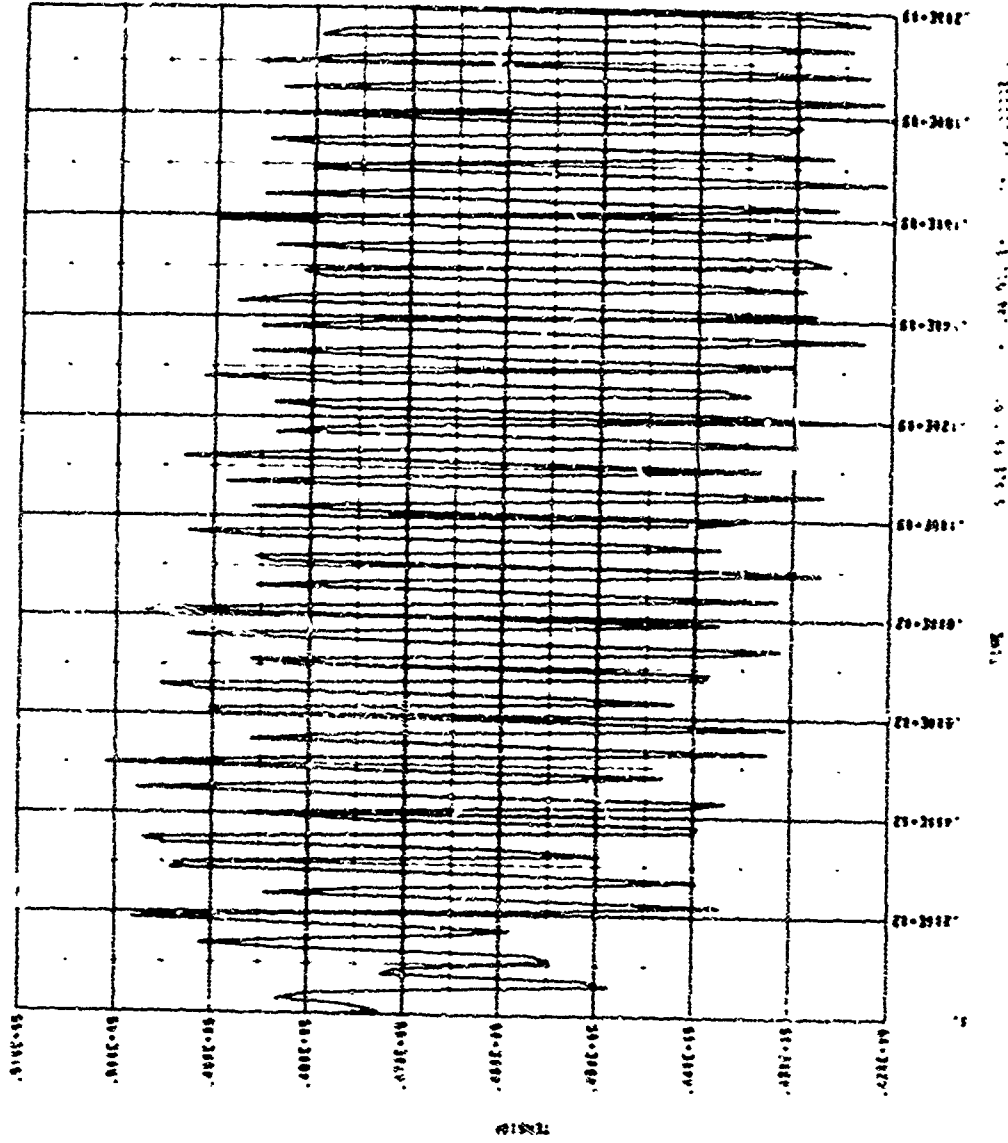
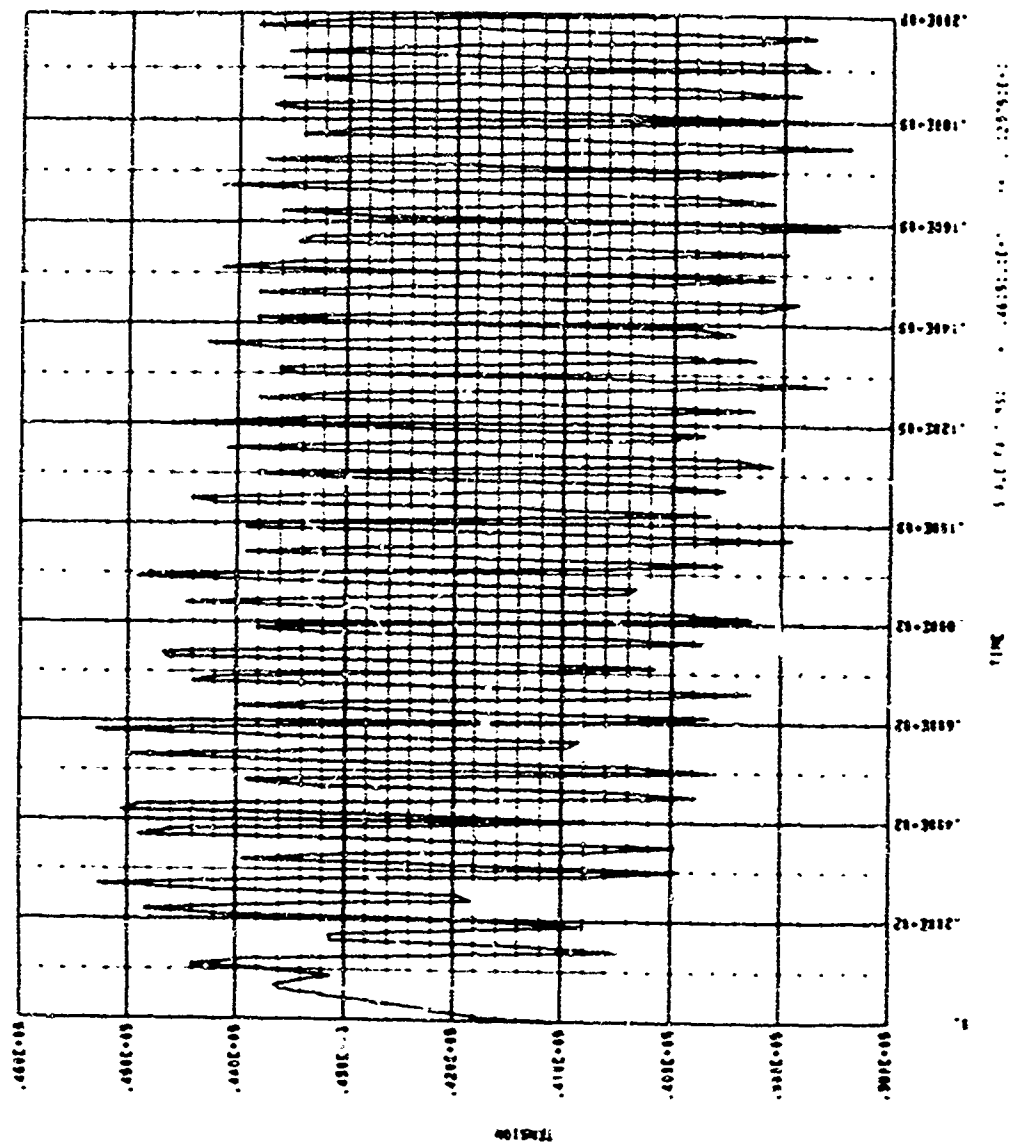


FIG. 79 TENSION AT THE BUOY. CONDITION 11. WAVE LENGTH = 145 FT. WAVE HEIGHT = 9.7 FT.

ANCHOR



POINT 302

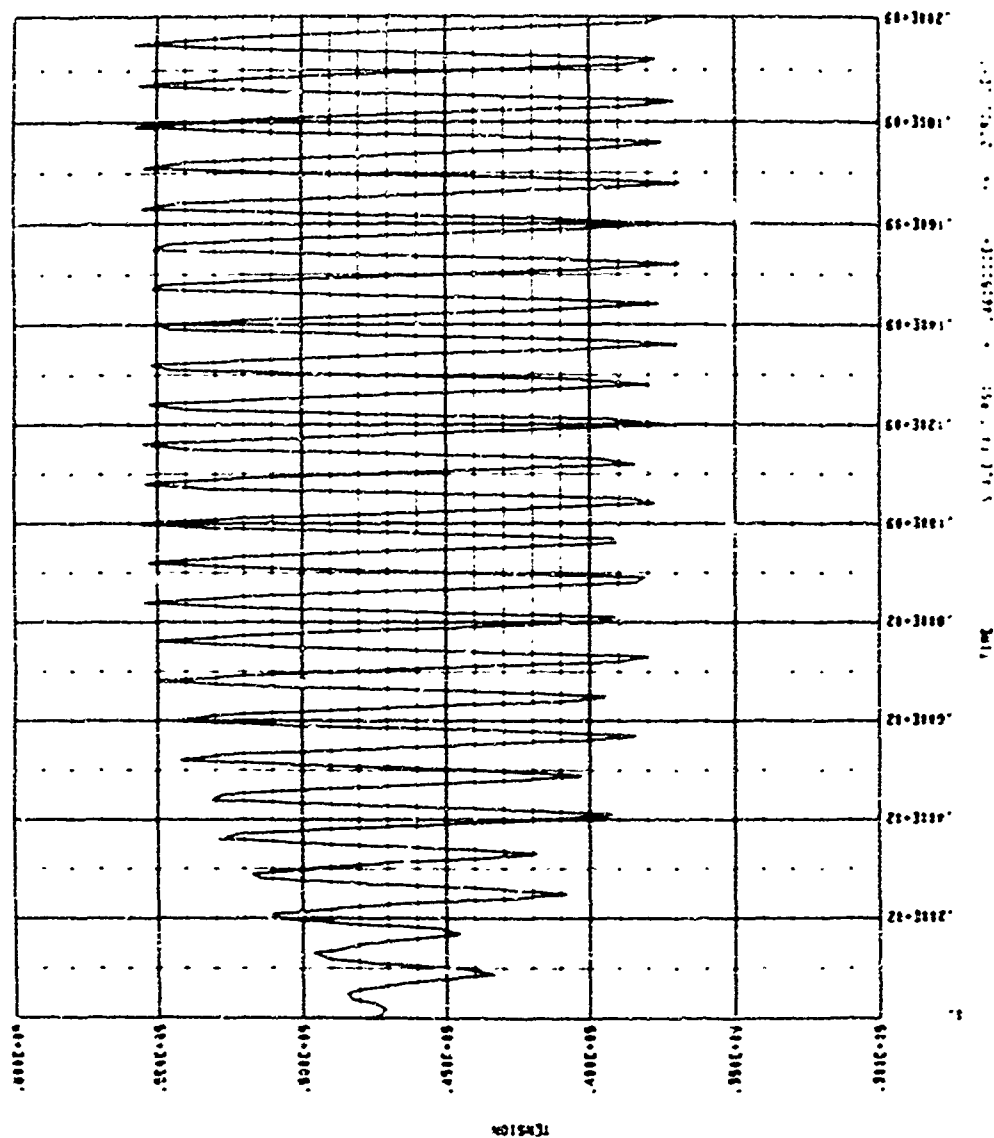
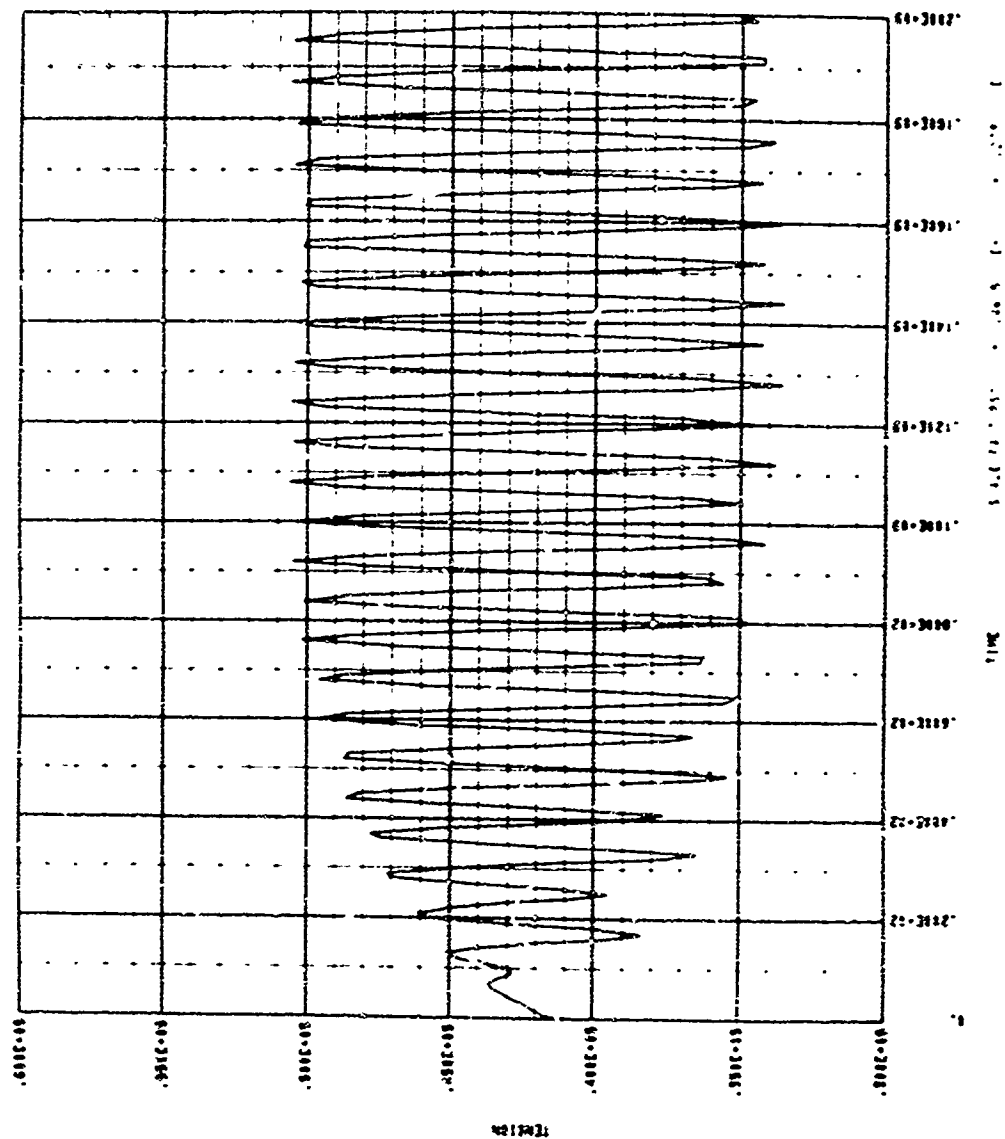


FIG. 21 TENSION AT THE BUOY. CONDITION II. WAVE LENGTH = 325 FT. WAVE HEIGHT = 21.7 FT.

ANCHOR



POINT 31A

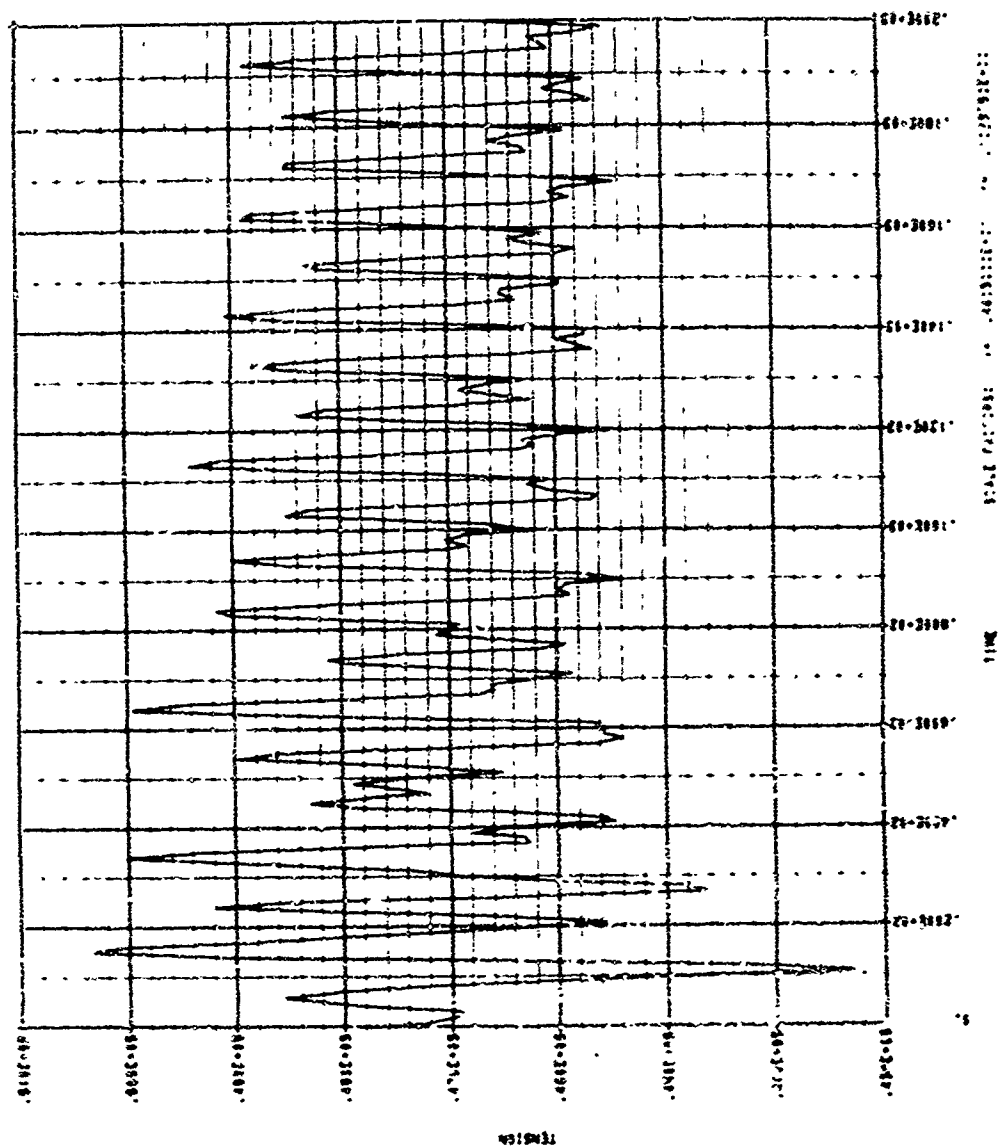


FIG. 23 TENSION AT THE BUOY. CONDITION II. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

ANCHOR

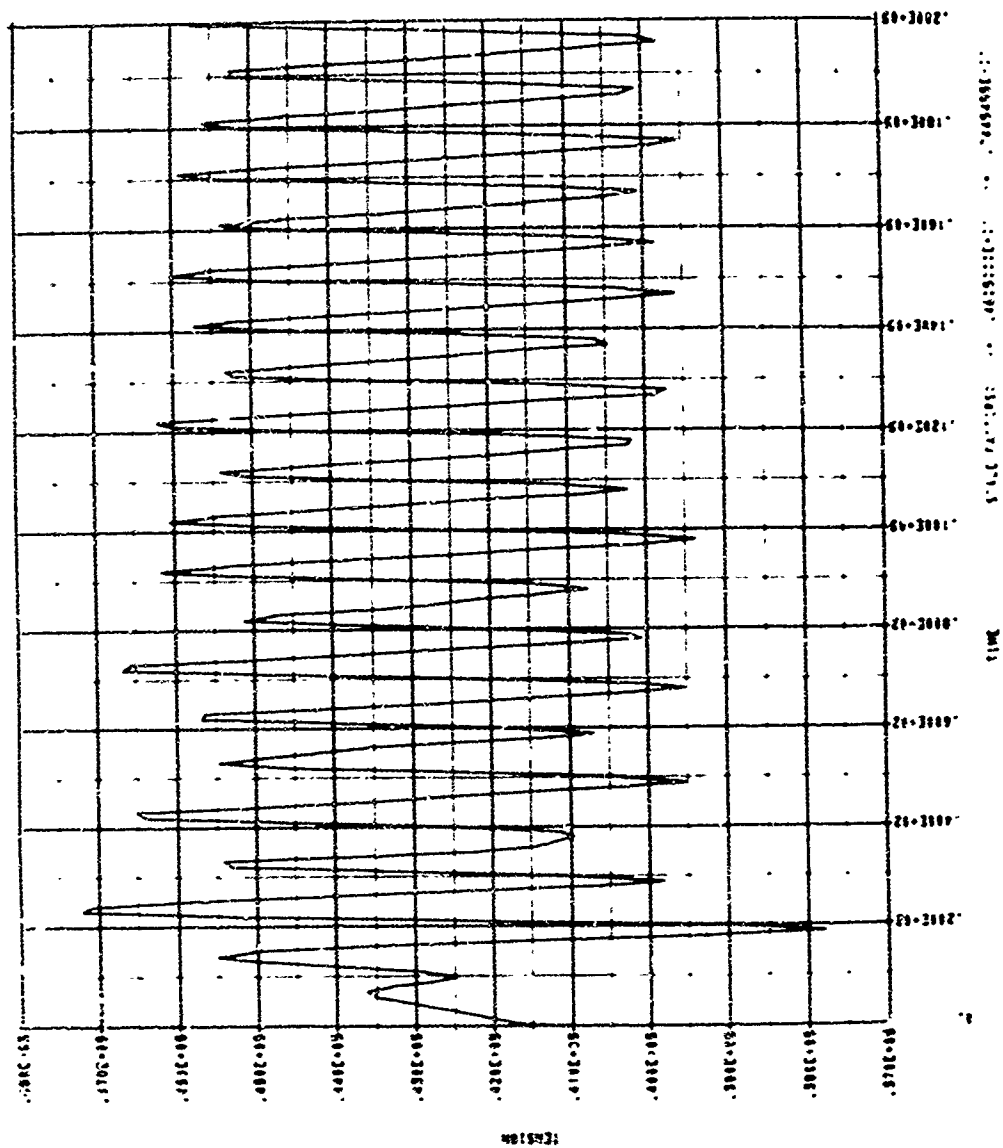


FIG. 24 TENSION AT THE ANCHOR. CONDITION II. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

POINT 31A

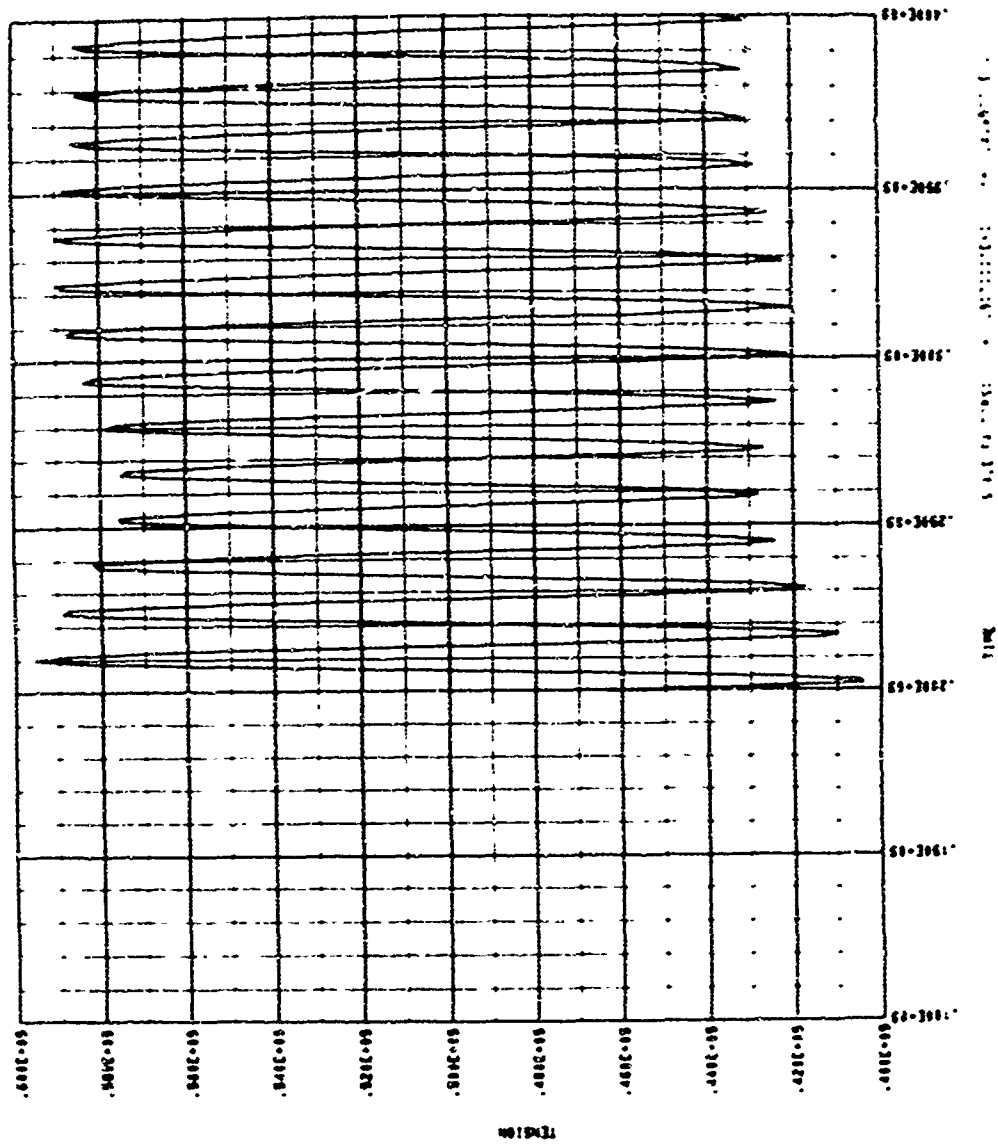


FIG. 25 TENSION AT THE BUOY. CONDITION II. WAVE LENGTH = 1000 FT. WAVE HEIGHT = 66.7 FT.

ANCHOR

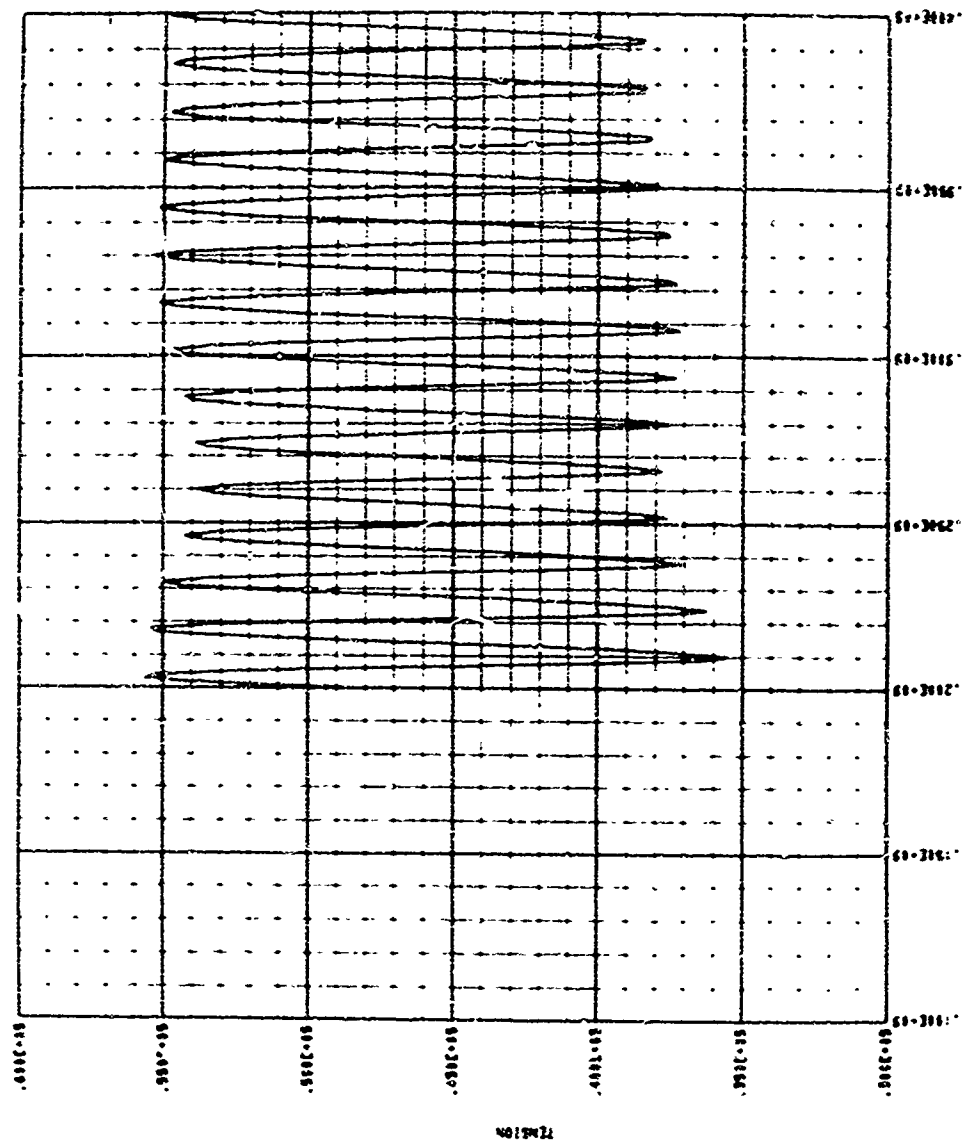


FIG. 26 TENSION AT THE ANCHOR. CONDITION II. WAVE LENGTH = 1000 FT. WAVE HEIGHT = 66.7 FT.

POINT 31A

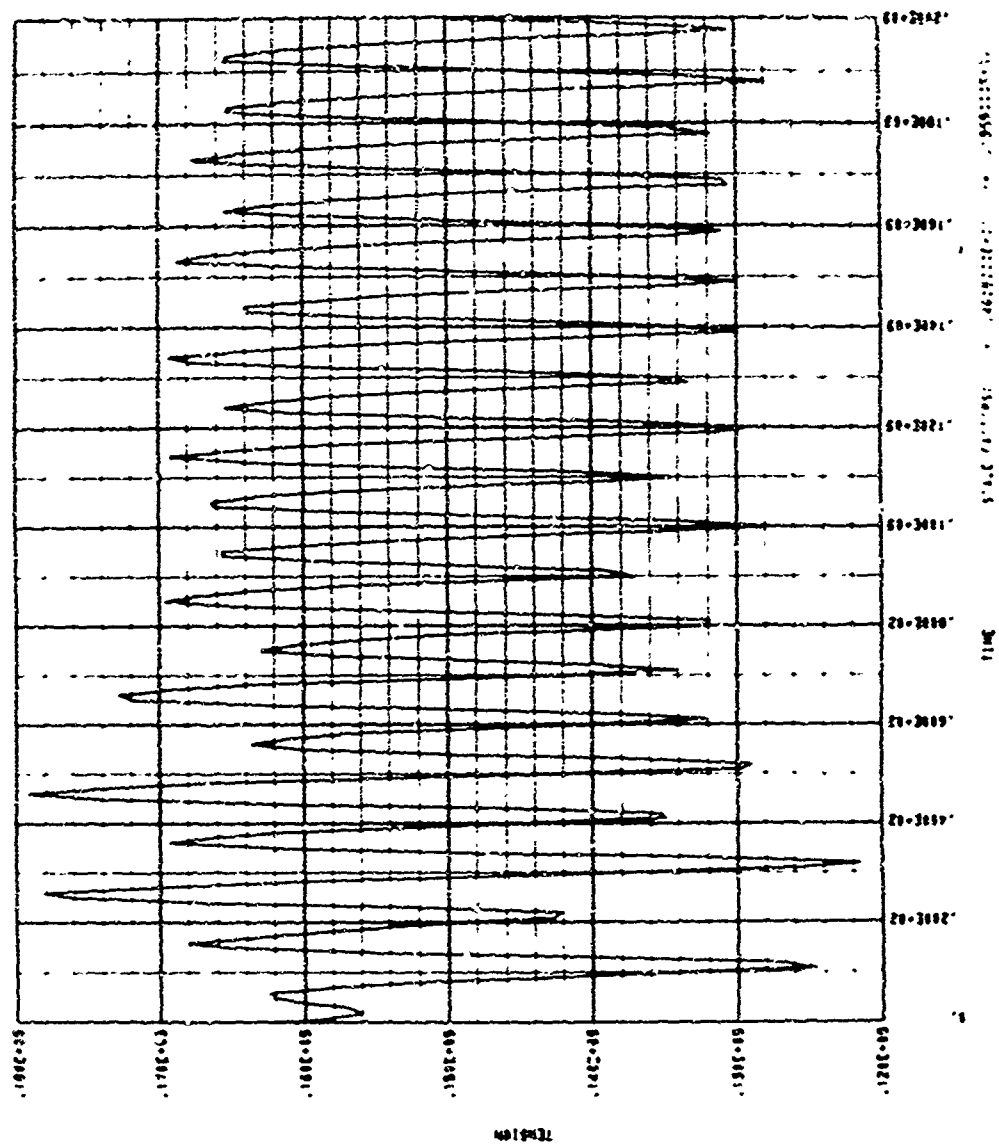


FIG. 27 TENSION AT THE BUOY. CONDITION III. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

ANCHOR

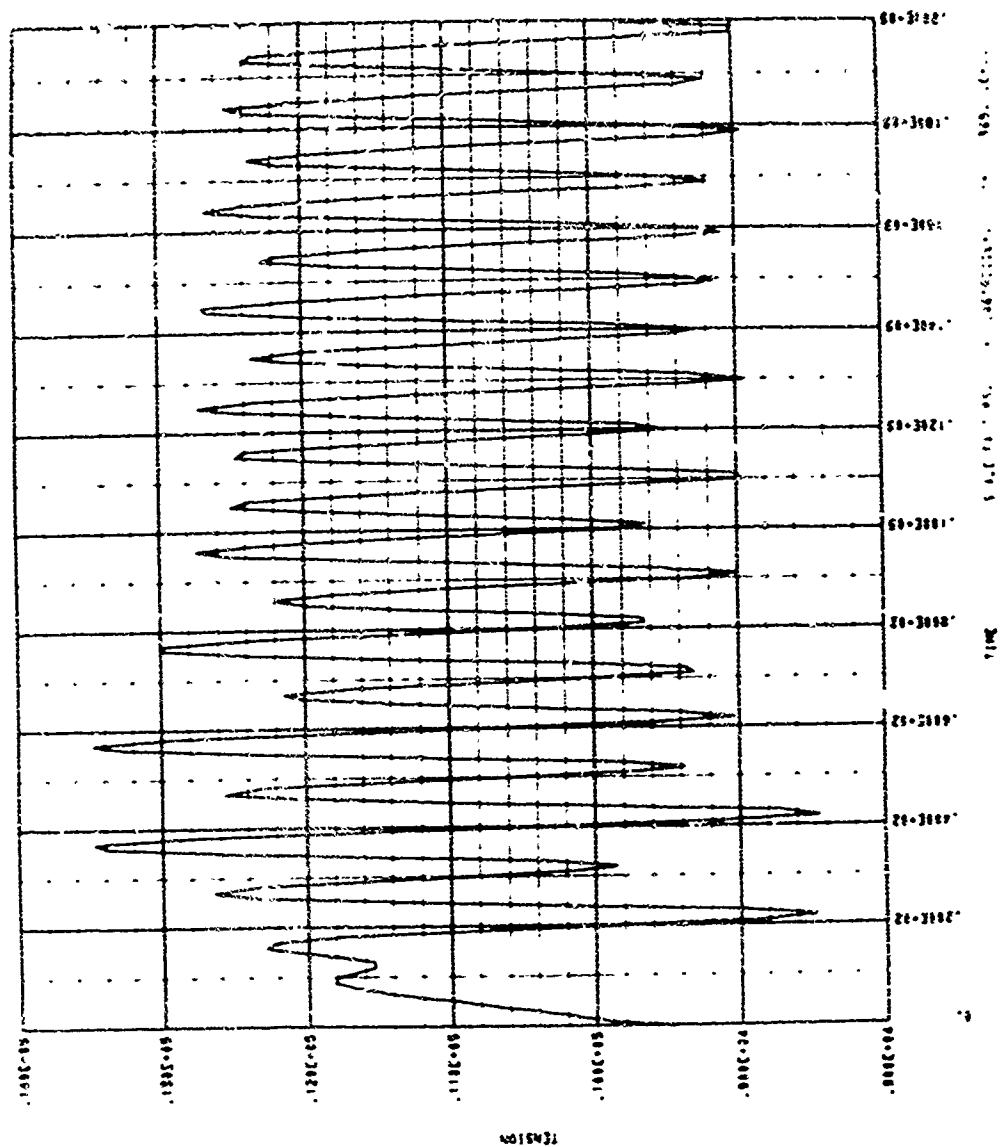


FIG. 28 TENSION AT THE ANCHOR. CONDITION III. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

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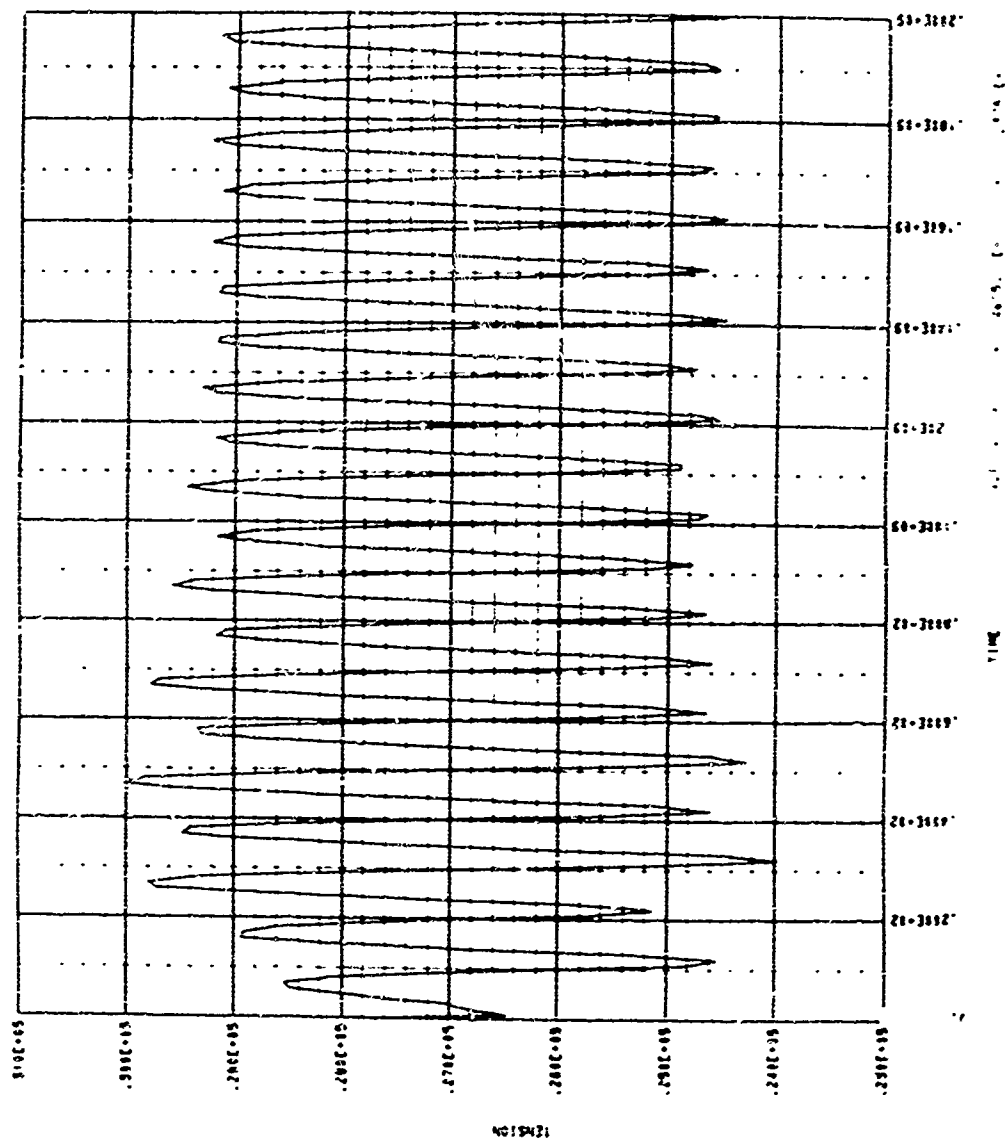


FIG. 29 TENSION AT THE BUOY. CONDITION IV. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

APCMCR

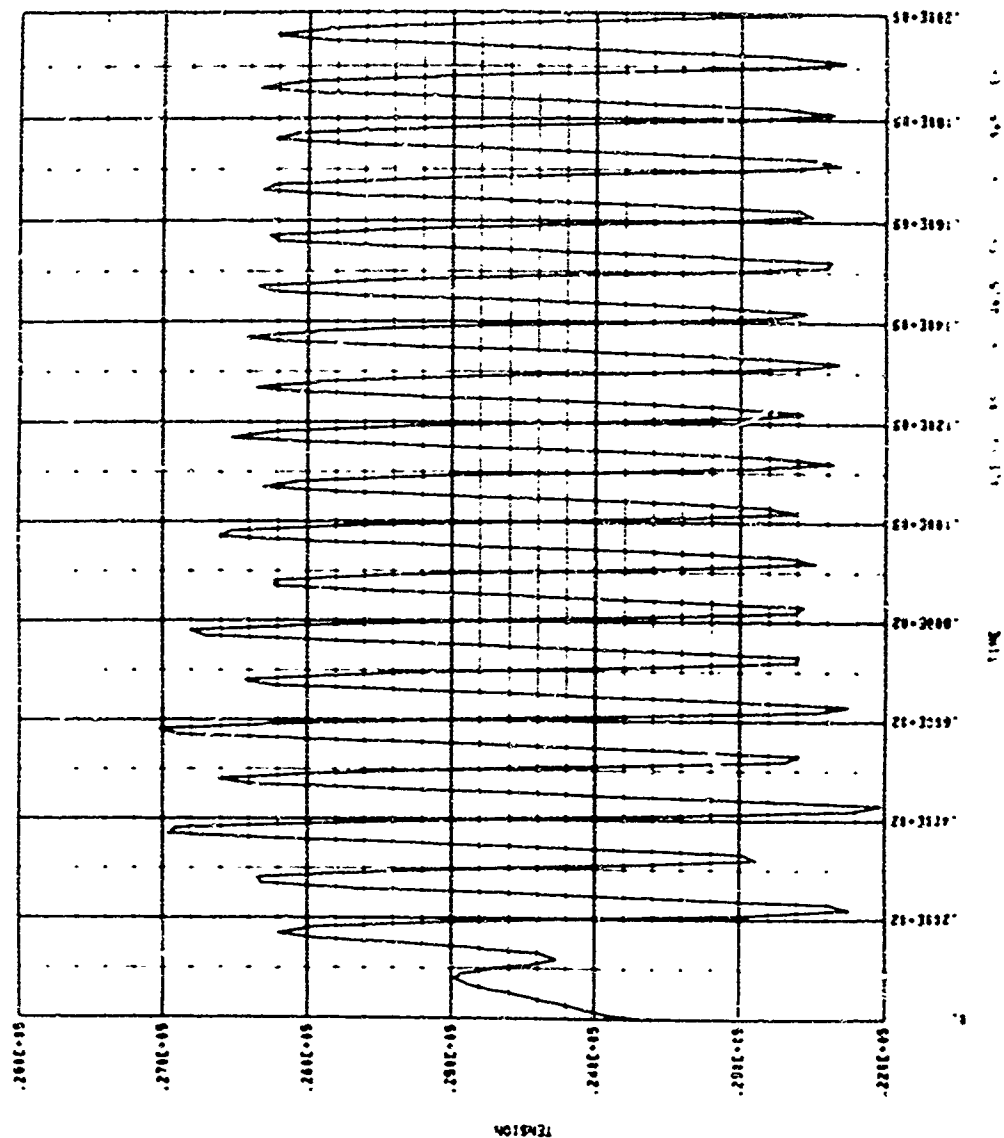


FIG. 30 TENSION AT THE ANCHOR. CONDITION IV. WAVE LENGTH = 500 FT. WAVE HEIGHT = 35.3 FT.

POINT 3-1

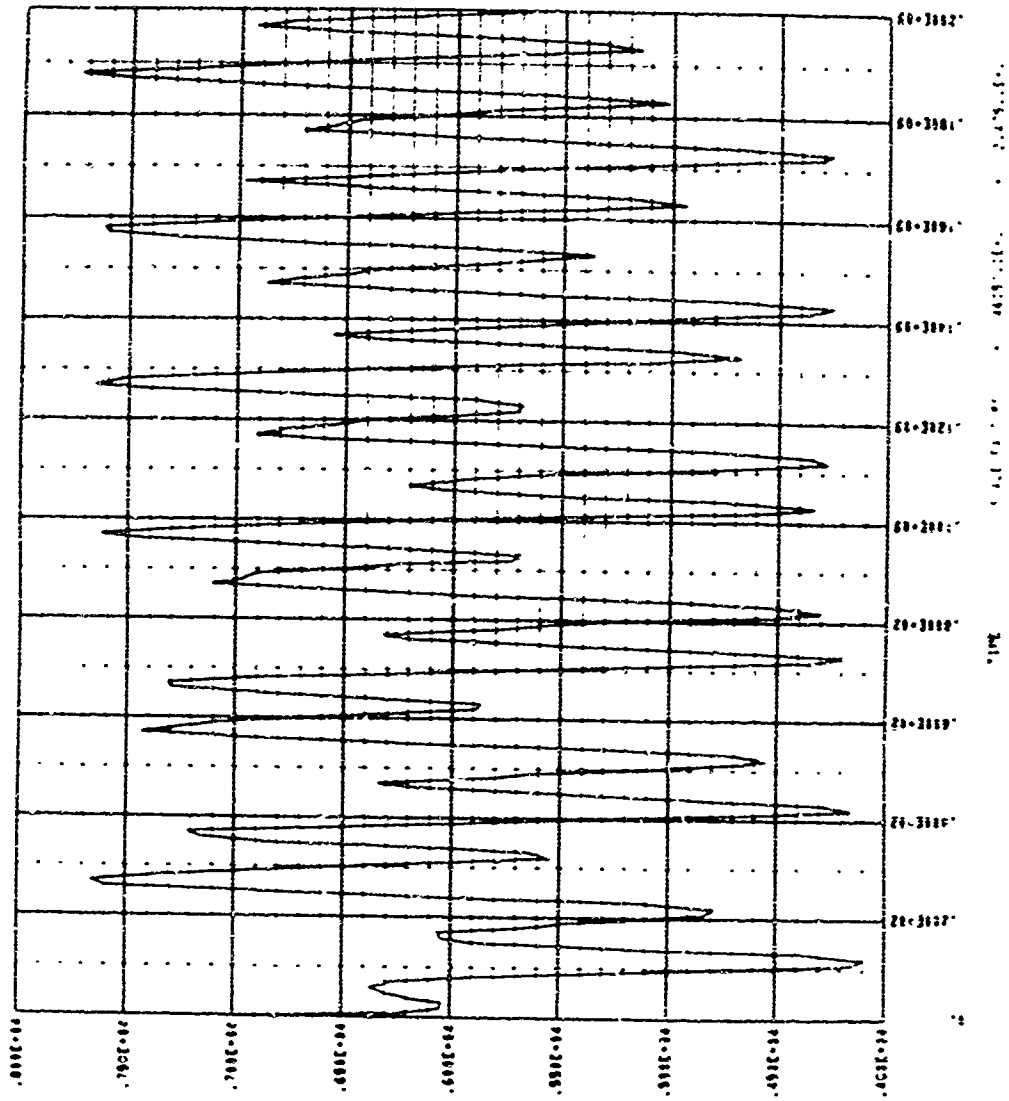


FIG. 31 TENSION AT THE BUOY. CONDITION V. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT

FIG. 32 TENSION AT THE ANCHOR. CONDITION V. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.5 FT.

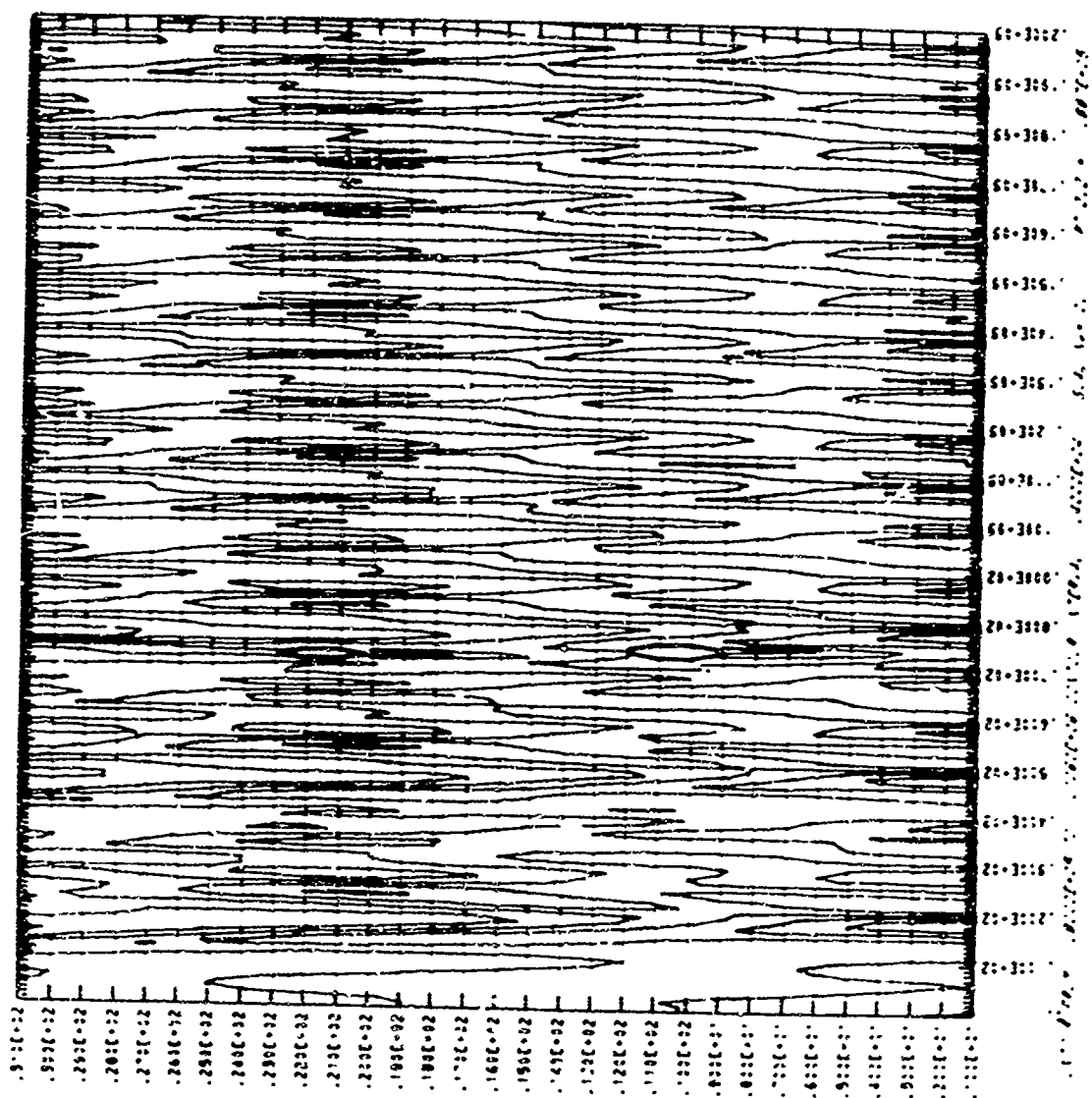


FIG. 33 TENSION CONTOURS. CONDITION I. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

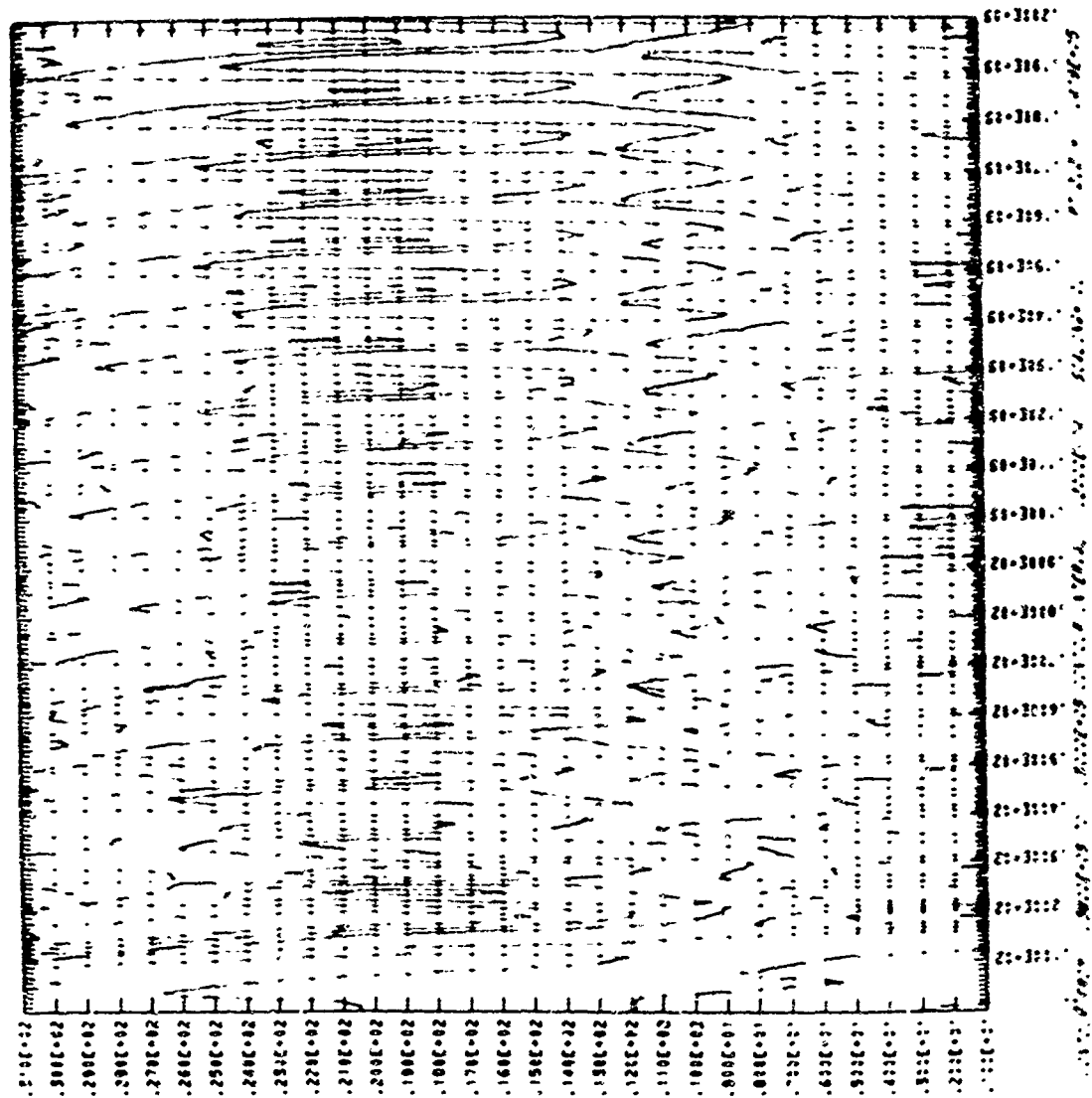


FIG. 34 TENSION CONTOURS. CONDITION II. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

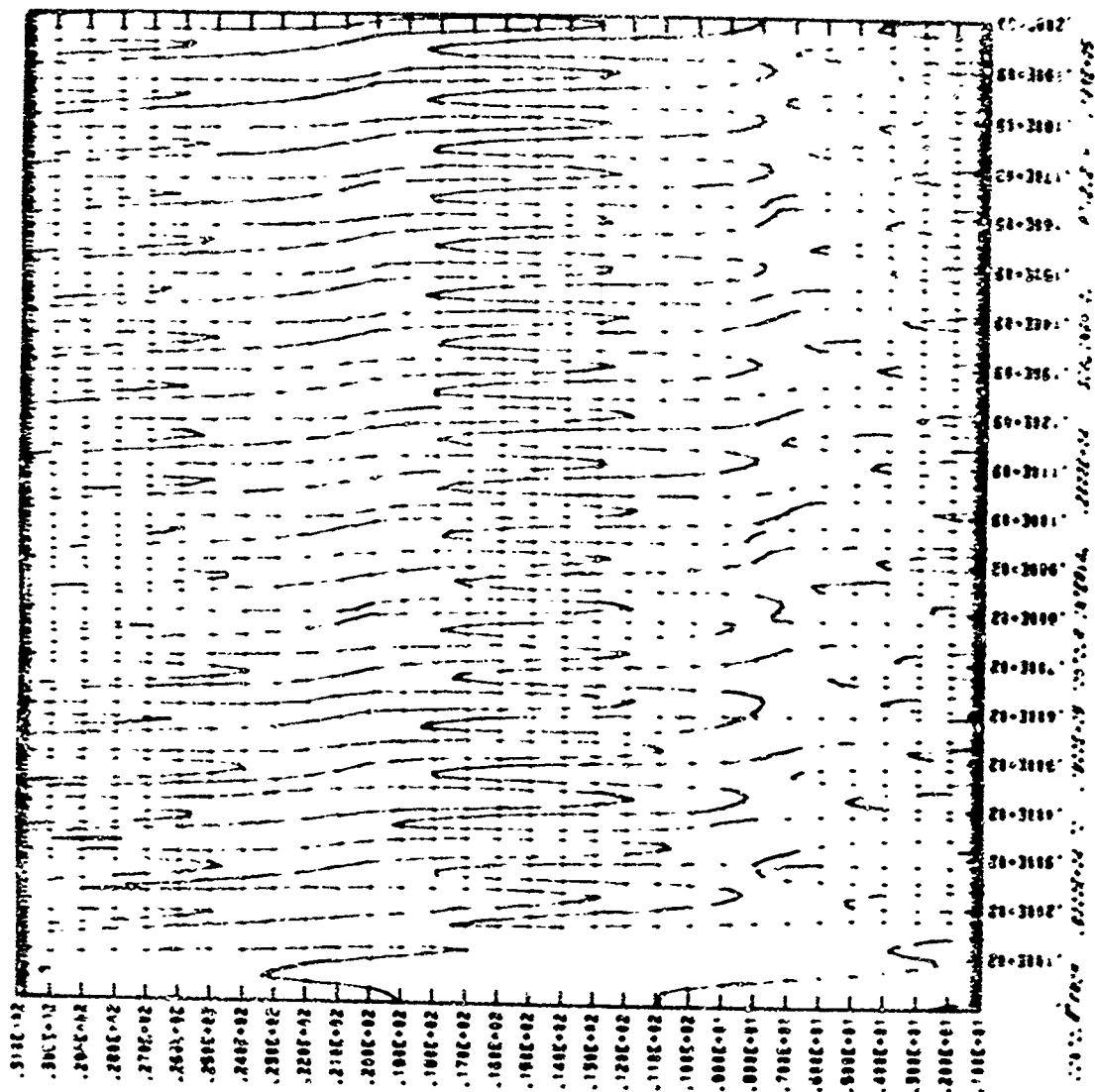


FIG. 35 TENSION CONTOURS. CONDITION III. WAVE LENGTH = 500 FT. WAVE HEIGHT = 53.3 FT.

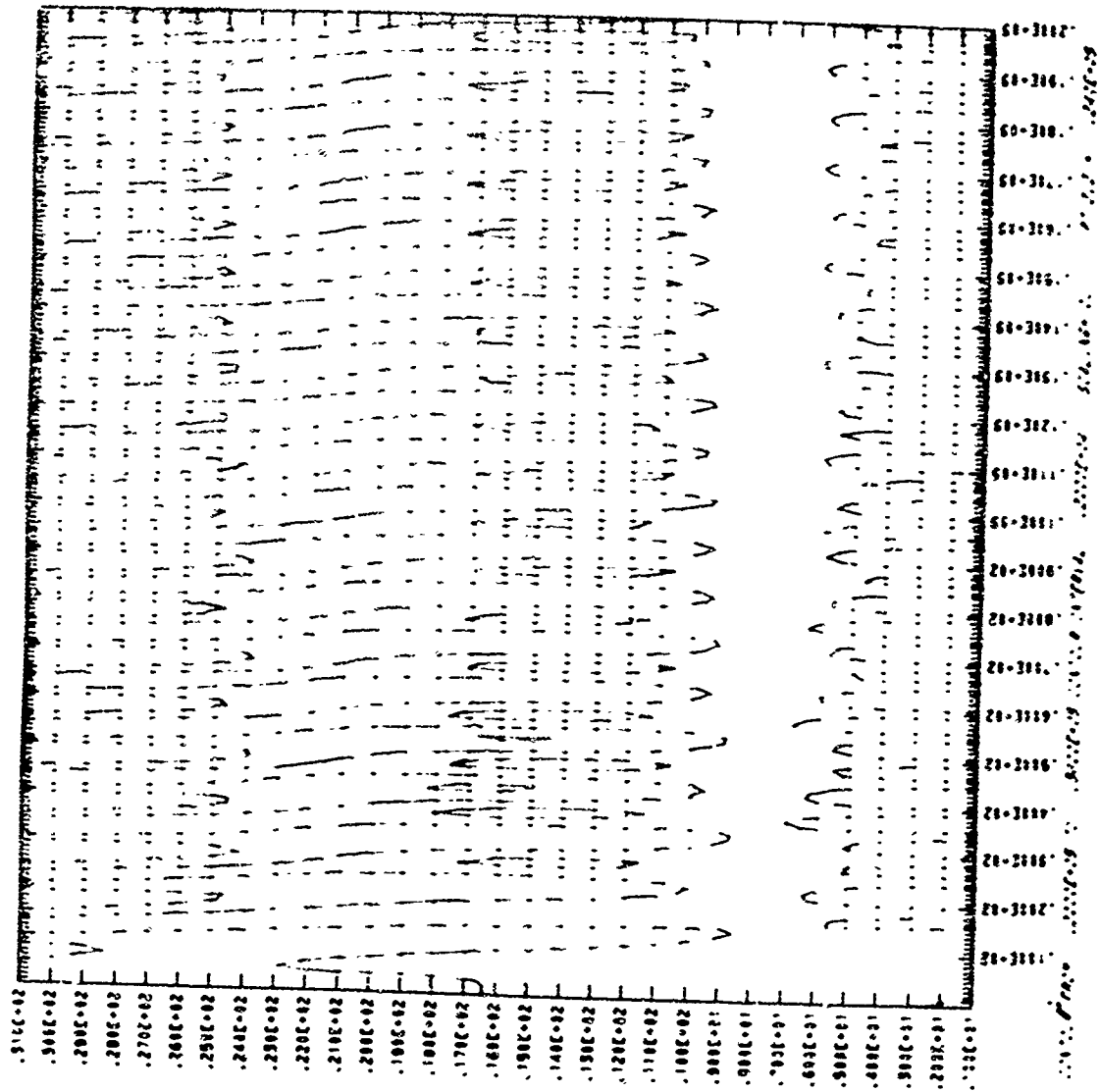


FIG. 36 TENSION CONTOURS. CONDITION IV. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

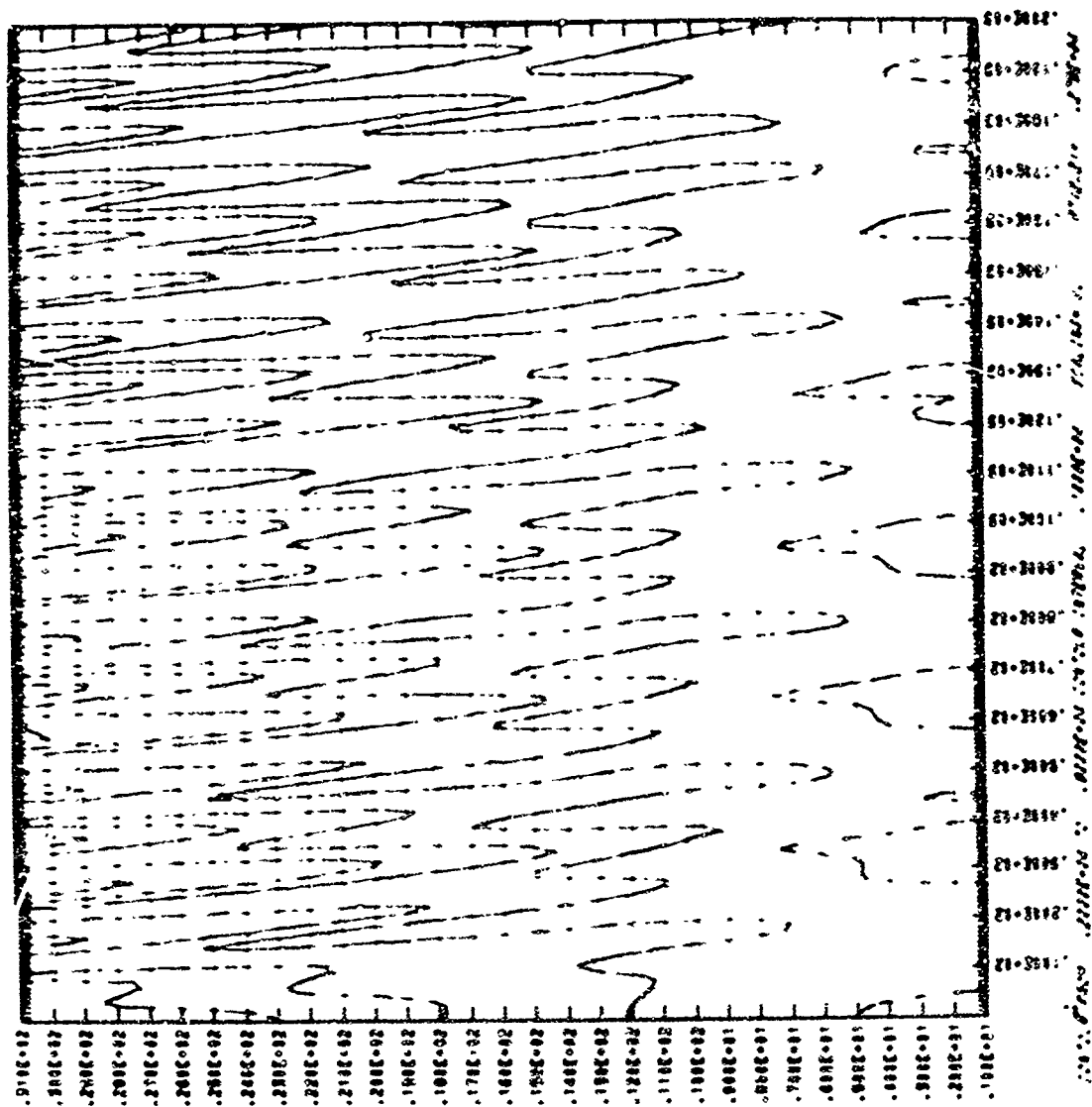


FIG. 37 TENSION CONTOURS. CONDITION V. WAVE LENGTH = 500 FT. WAVE HEIGHT = 33.3 FT.

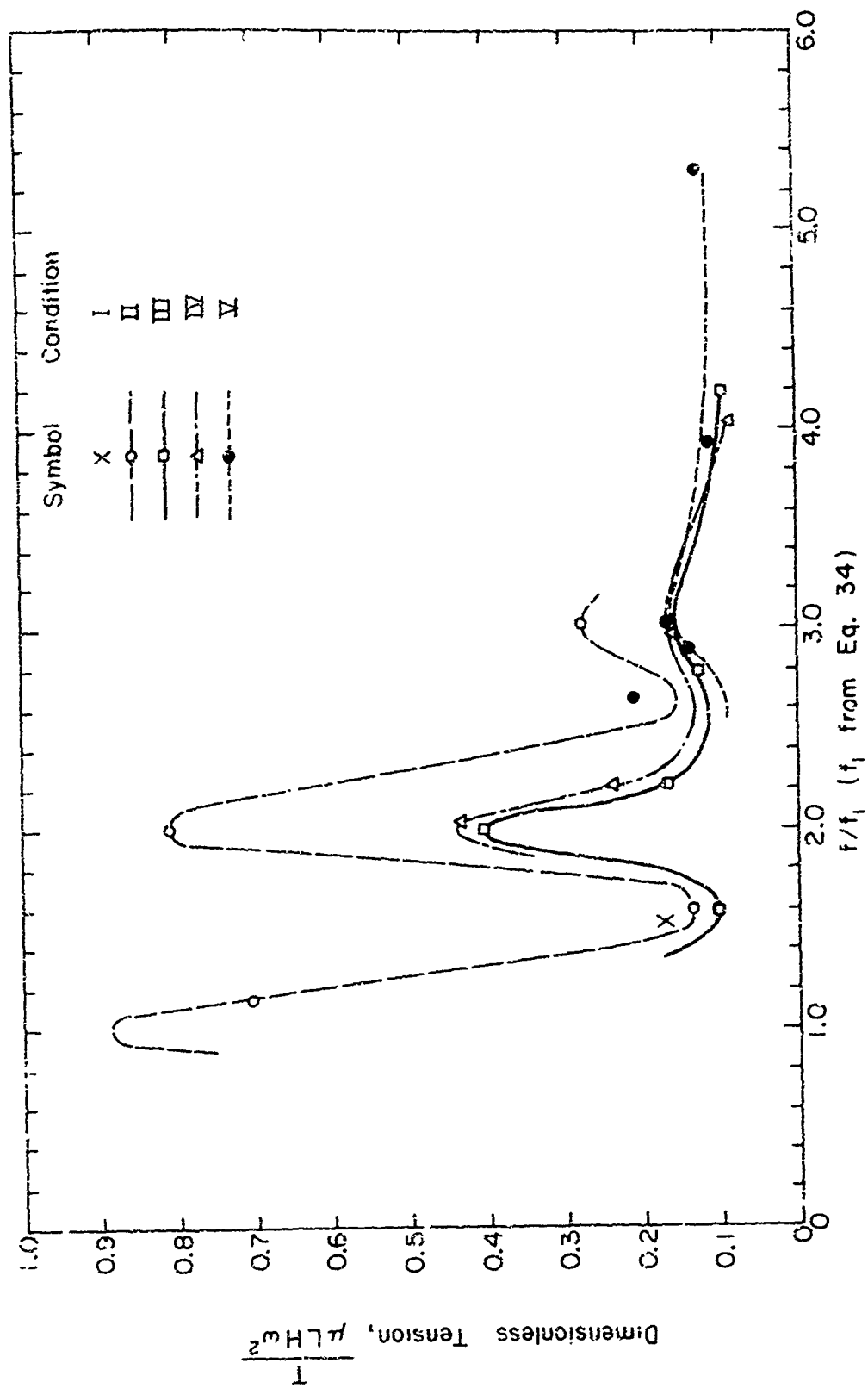


FIG. 38 ESTIMATED FREQUENCY RESPONSE CURVES FOR LINE TENSION AT THE BUOY. DEPTH = 20,000 FT.

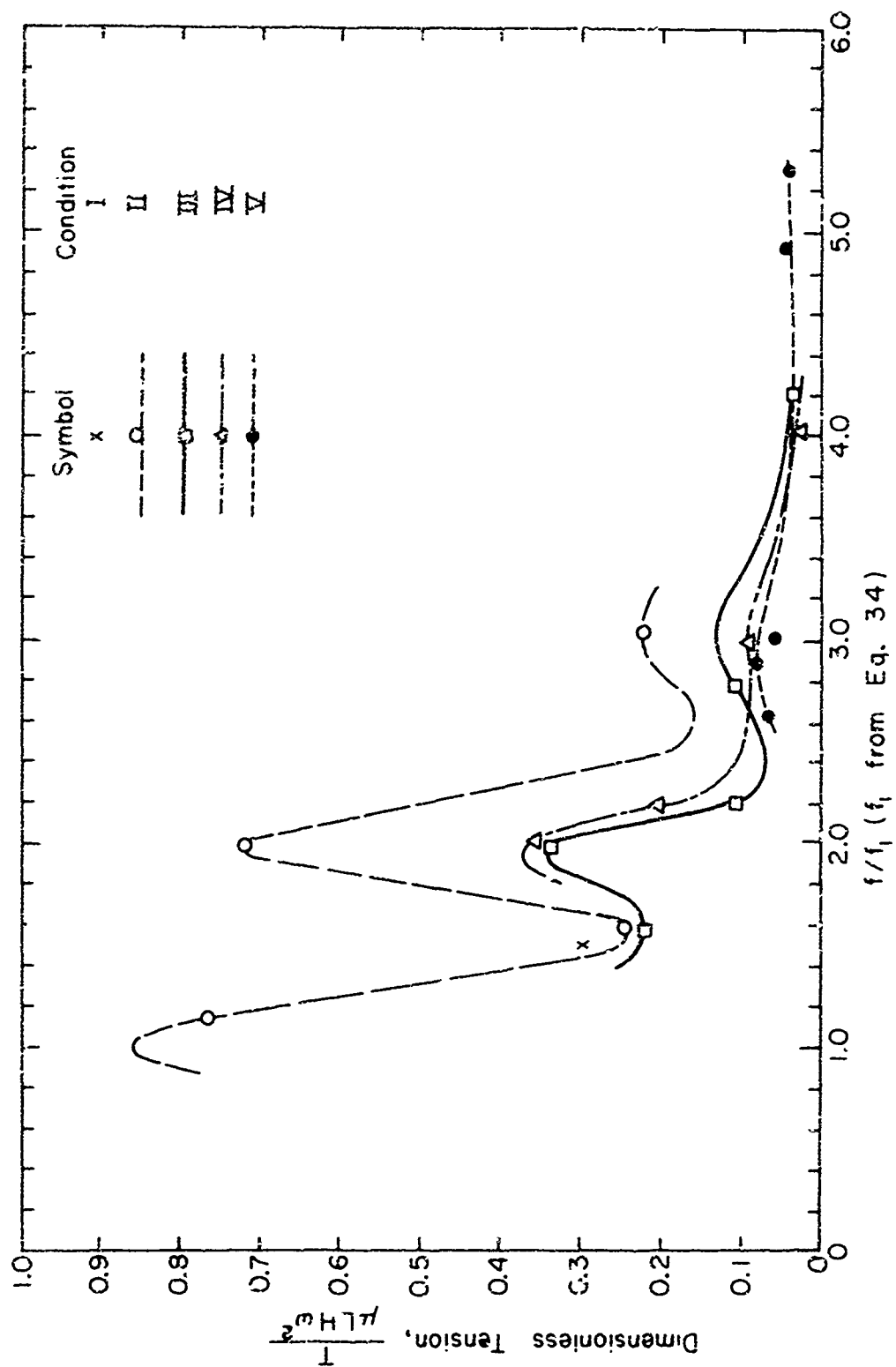


FIG. 39 ESTIMATED FREQUENCY RESPONSE CURVES FOR LINE TENSION AT THE ANCHOR. DEPTH = 20,000 FT.

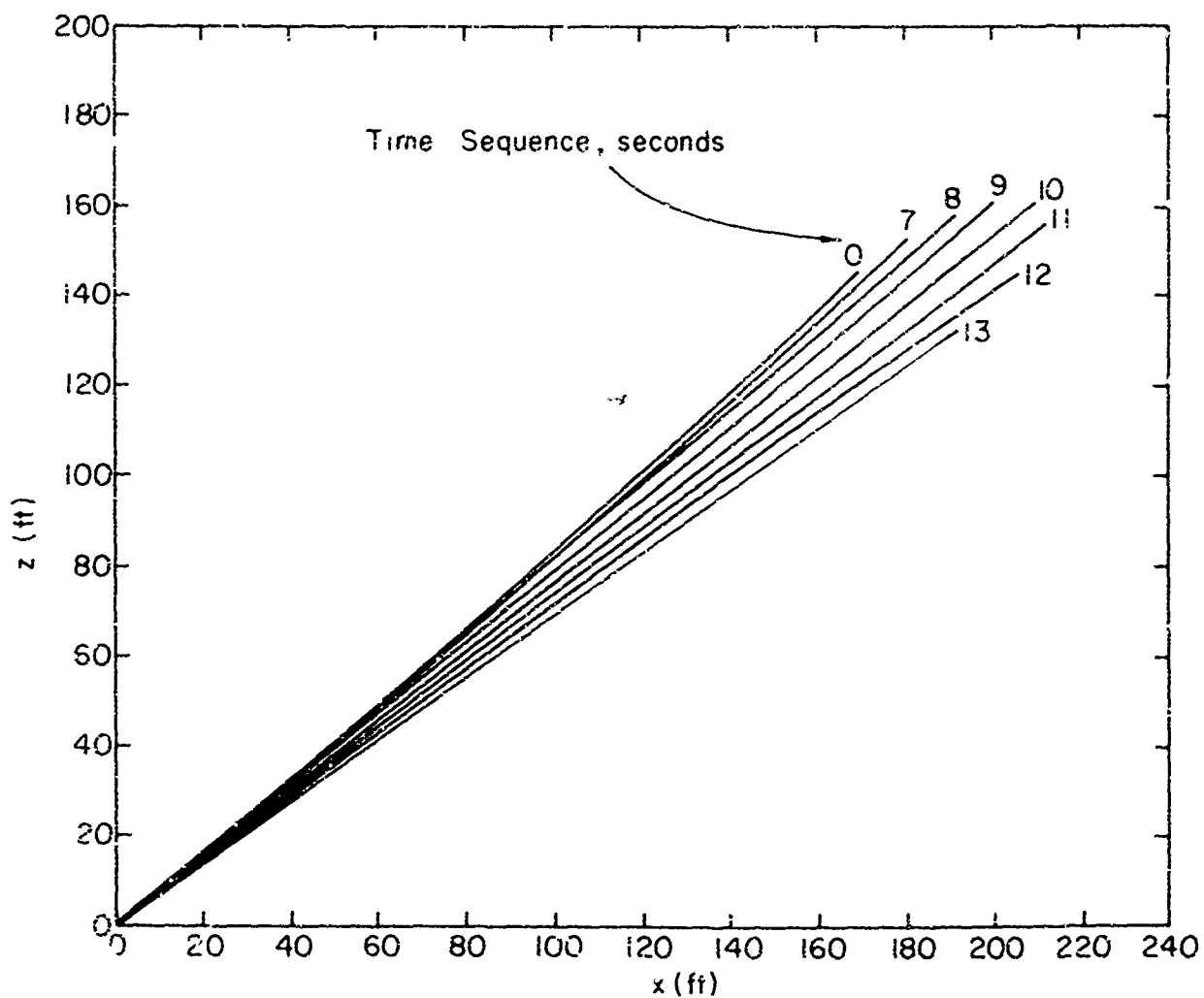


FIG. 40 SEQUENTIAL POSITIONS OF THE MOORING LINE. DEPTH = 150 FT. WAVE LENGTH = 600 FT. WAVE HEIGHT = 40 FT. WIND = 50 KTS.

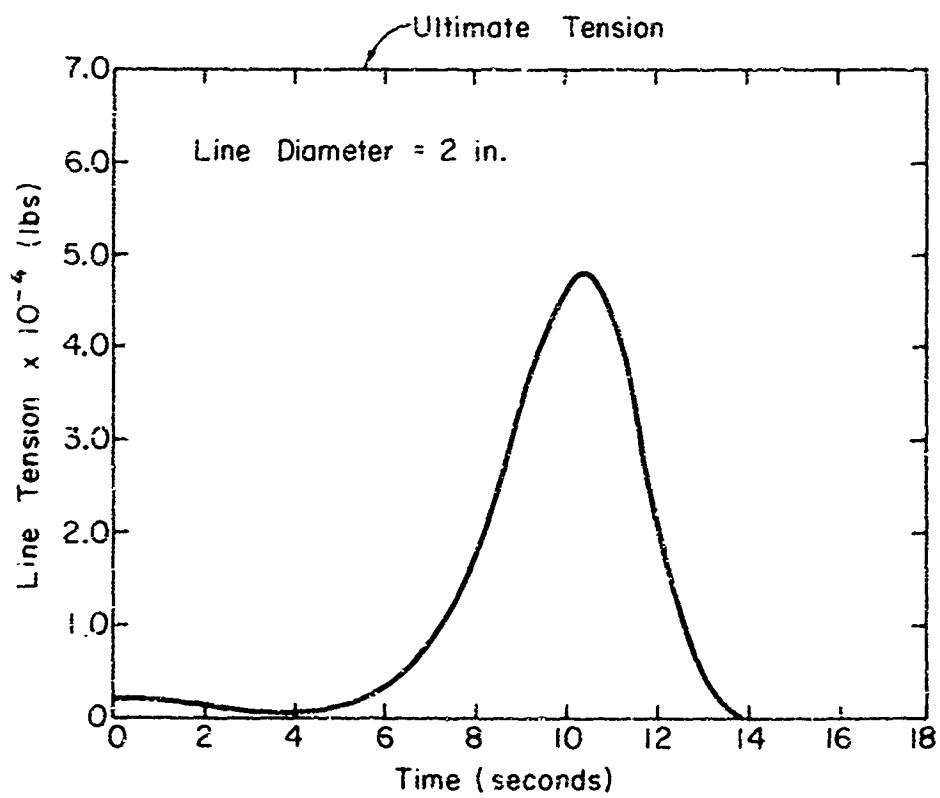


FIG. 41 MOORINGS LINE TENSION. DEPTH = 150 FT. WAVE LENGTH = 600 FT. WAVE HEIGHT = 40 FT. WIND = 50 KTS.

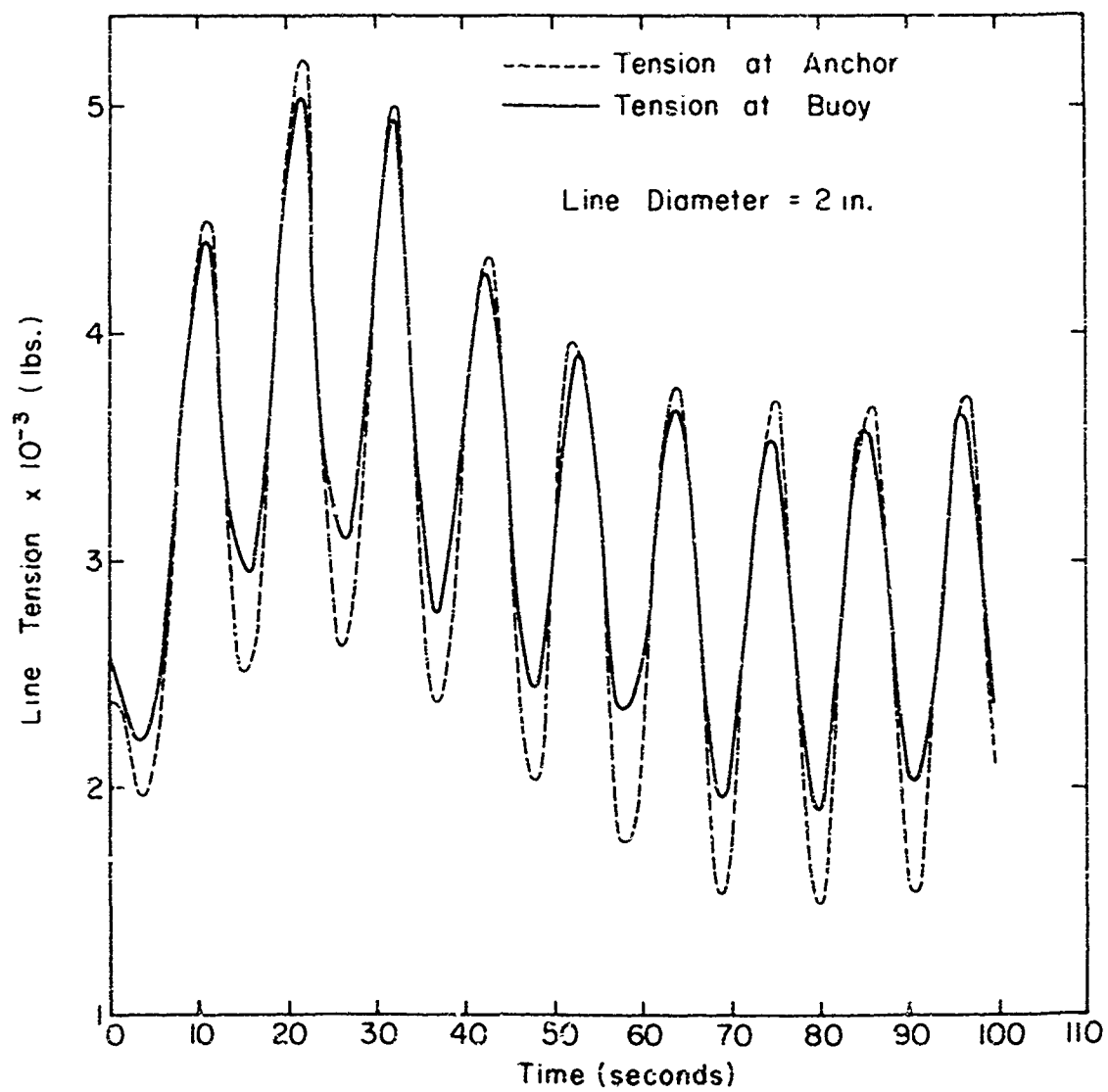


FIG. 42 MOORING LINE TENSION. DEPTH = 100 FT. WAVE LENGTH = 600 FT. WAVE HEIGHT = 40 FT. WIND = 50 KTS.